

**Fuel-Cycle Energy and Emission Impacts of Ethanol-Diesel Blends in  
Urban Buses and Farming Tractors**

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## Acronyms

2WD	two-wheel drive
4WD	four-wheel drive
ADM	Archer Daniels Midland
AAPFCO	Association of American Plant Food Control Officials
CD	conventional diesel
CH <sub>4</sub>	methane
CO	carbon monoxide
CO <sub>2</sub>	carbon dioxide
DCCA	Illinois Department of Commerce and Community Affairs
DOE	U.S. Department of Energy
E10	10% ethanol and 90% gasoline by volume
ED	ethanol-diesel blend
ED7.5	7.5% ethanol and 92.5% diesel by volume
ED10	10% ethanol and 90% diesel by volume
ED15	15% ethanol and 85% diesel by volume
E-diesel	ethanol-diesel blend
EFMA	European Fertilizer Manufacturers Association
EPA	U.S. Environmental Protection Agency
FC	fuel consumption
GHG	greenhouse gases
REET	Greenhouse gases, Regulated Emissions, and Energy use in Transportation
GWP	global warming potential
HC	hydrocarbon
HHV	higher heating value
HNO <sub>3</sub>	nitric acid
H <sub>2</sub> SO <sub>4</sub>	sulfuric acid
IPCC	Intergovernmental Panel on Climate Change
K <sub>2</sub> O	potassium oxide (potash)
LHV	lower heating value
LPG	liquefied petroleum gas
LS	low-sulfur
LSD	low-sulfur diesel
MTBE	methyl tertiary butyl ether
N	nitrogen
NAFTA	North American Free Trade Association
NG	natural gas
NH <sub>3</sub>	ammonia
N <sub>2</sub> O	nitrous oxide
NO <sub>x</sub>	nitrogen oxides
OTT	Office of Transportation Technologies
P <sub>5</sub> O <sub>2</sub>	phosphorus oxide (phosphate)
PM	particulate matter
PM <sub>10</sub>	particulate matter with diameter 10 microns or smaller
PTW	pump-to-wheels
RFS	renewable fuels standard

S	sulfur
SO <sub>x</sub>	sulfur oxides
SwRI	Southwest Research Institute
TFI	The Fertilizer Institute
THC	total hydrocarbon
TOC	total organic compounds
USDA	U.S. Department of Agriculture
VOC	volatile organic compounds
PTW	pump-to-wheels
WTP	well-to-pump
WTW	well-to-wheels

### **Units of Measure**

Btu	British thermal unit
g	gram
gal	gallon
hp	horsepower
hr	hour
kg	kilogram
lb	pound
mi	mile
mmBtu	million Btu
ppm	parts per million
rpm	revolutions per minute
yr	year

## **Introduction**

About 2.1 billion gallons of fuel ethanol was used in the United States in 2002, mainly in the form of gasoline blends containing up to 10% ethanol (E10). Ethanol use has the potential to increase in the U.S. blended gasoline market because methyl tertiary butyl ether (MTBE), formerly the most popular oxygenate blendstock, may be phased out owing to concerns about MTBE contamination of the water supply. Ethanol would remain the only viable near-term option as an oxygenate in reformulated gasoline production and to meet a potential federal renewable fuels standard (RFS) for transportation fuels. Ethanol may also be blended with additives (co-solvents) into diesel fuels for applications in which oxygenation may improve diesel engine emission performance.

Numerous studies have been conducted to evaluate the fuel-cycle energy and greenhouse gas (GHG) emission effects of ethanol-gasoline blends relative to those of gasoline for applications in spark-ignition engine vehicles (see Wang et al. 1997; Wang et al. 1999; Levelton Engineering et al. 1999; Shapouri et al. 2002; Graboski 2002). Those studies did not address the energy and emission effects of ethanol-diesel (E-diesel or ED) blends relative to those of petroleum diesel fuel in diesel engine vehicles. The energy and emission effects of E-diesel could be very different from those of ethanol-gasoline blends because (1) the energy use and emissions generated during diesel production (so-called "upstream" effects) are different from those generated during gasoline production; and (2) the energy and emission performance of E-diesel and petroleum diesel fuel in diesel compression-ignition engines differs from that of ethanol-gasoline blends in spark-ignition (Otto-cycle-type) engine vehicles.

The Illinois Department of Commerce and Community Affairs (DCCA) commissioned Argonne National Laboratory to conduct a full fuel-cycle analysis of the energy and emission effects of E-diesel blends relative to those of petroleum diesel when used in the types of diesel engines that will likely be targeted first in the marketplace. This report documents the results of our study. The draft report was delivered to DCCA in January 2003. This final report incorporates revisions by the sponsor and by Argonne.

## **Study Scope**

In the past several years, test bench experiments and fleet demonstrations using E-diesel in diesel engines have been conducted in the United States and in other countries. Although both diesel passenger cars and diesel heavy trucks were tested with E-diesel, application of E-diesel in the United States will very likely be concentrated in subsets of the heavy vehicle fleet. So the present study does not encompass E-diesel use in diesel passenger cars, but focuses on urban transit buses and farming tractors, which are likely to be among the earliest commercial E-diesel applications. In past and current U.S. demonstration programs, buses and farming tractors operate on E-diesel blends. Besides the petroleum displacement advantage, use of E-diesel in urban buses is intended primarily to help reduce emissions of fine particulate matter (PM) and oxides of nitrogen (NO<sub>x</sub>); PM has been identified as an important direct health threat and NO<sub>x</sub> as an important precursor of tropospheric ozone. The application of E-diesel in farming tractors is viewed by the agricultural community as a means to use an agriculture-based fuel for farming activities.

To this point, experiments have involved ethanol blended into diesel at proportions between 7.5% and 15% by volume (ED7.5 to ED15). In order to avoid phase separation, fuel additives are used in ED

blends. Several vendors currently produce and supply proprietary additives for ethanol and diesel blending. For ED blends ranging from 7.5% to 15%, the treat rate of additives ranges from about 1% to 1.5% by volume. In general, these rates are significantly lower than in earlier ED blends. We have included estimates of the energy use and emissions associated with additive production and distribution in our fuel-cycle analysis.

The U.S. Environmental Protection Agency (EPA) has adopted a low-sulfur (LS) diesel requirement that will begin to be phased in 2006. The new regulations will require that diesel fuel with a maximum sulfur (S) content of 15 ppm (by weight) represent 100% of the diesel fuel supply for on-road vehicles by 2009. So LS diesel is assumed for urban bus applications in this study. By contrast, the off-road diesel used in farming tractors currently has very high sulfur content, often in excess of 3,000 ppm by weight. EPA intends to regulate the sulfur content of off-road diesel, but at this time, it is not clear what the mandated sulfur limit will be. We have assumed that the current on-road diesel, with an average 350-ppm sulfur content, will be used in future farming tractors. Table 1 lists the vehicle and fuel options evaluated in this study.

**Table 1.** Vehicle and Fuel Options Evaluated in This Study

<b>Fuel</b>	<b>Urban Buses</b>	<b>Farming Tractors</b>
Baseline fuel	15-ppm-S diesel	350-ppm-S diesel
Ethanol diesel blends (by volume)		
ED10	10% ethanol, 89% 15-ppm-S diesel, and 1% additive	10% ethanol, 89% 350-ppm-S diesel, and 1% additive
ED15	15% ethanol, 83.5% 15-ppm-S diesel, and 1.5% additive	15% ethanol, 83.5% 350-ppm-S diesel, and 1.5% additive

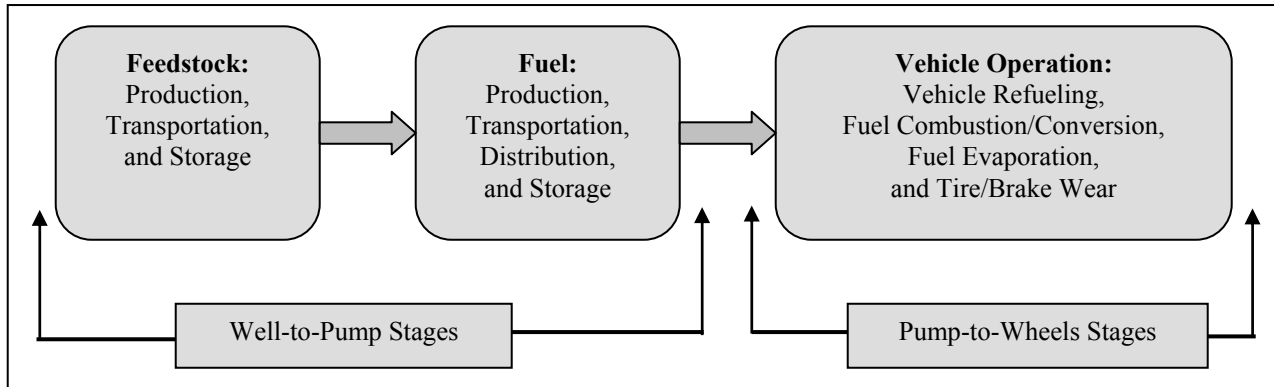
## Methodology

Crop-based production of ethanol for blending with diesel fuel is distinctly different from petroleum-based production of diesel. Although ethanol itself is a renewable fuel, the production of corn and ethanol requires the use of fossil energy and generates GHG emissions. A complete evaluation of E-diesel vs. petroleum diesel requires a full fuel-cycle, or "well-to-wheels" (WTW), analysis. Argonne has conducted WTW analyses of ethanol/gasoline blends relative to gasoline (Wang et al. 1997; Wang et al. 1999). This study analyzes WTW energy and GHG emission effects of E-diesel vs. petroleum diesel by using a method identical to that used in the 1997 and 1999 studies, but with updated data on the energy use associated with fertilizer manufacture, corn farming, and ethanol production and on N<sub>2</sub>O emissions from cornfields.

A WTW analysis of a vehicle/fuel system covers all stages of the fuel cycle — from energy feedstock recovery (wells) to energy delivered at vehicle wheels (wheels). Since 1995, with funding from the U.S. Department of Energy's (DOE's) Office of Transportation Technologies (OTT), Argonne has been developing the Greenhouse gases, Regulated Emissions, and Energy use in Transportation (GREET) model as an analytical tool for use by researchers and practitioners to estimate WTW energy use and emissions associated with transportation fuels and advanced vehicle technologies. Argonne released the first version of the GREET model in June 1996 (Wang 1996). Since then,<sup>6</sup>

Argonne has released a series of GREET versions (Wang 1999; Wang 2001; General Motors Corporation et al. 2001a, b, c). The GREET model and associated documents are posted on Argonne’s GREET website at <http://greet.anl.gov>.

Figure 1 presents the stages and activities covered in GREET’s WTW simulations of vehicle/fuel systems. A WTW analysis includes the feedstock, fuel, and vehicle operation stages. The feedstock and fuel stages together are called “well-to-pump” (WTP) or “upstream” stages, and the vehicle operation stage is called the “pump-to-wheels” (PTW) or “downstream” stage. In GREET, WTW energy use and emission results are presented separately for each of the three stages shown in Figure 1.



**Figure 1.** Well-to-Wheels Stages of Vehicle/Fuel Systems Covered in the GREET Model

In our WTW analyses, as in many other similar studies, we include energy use and emissions for operation stages only. That is, any activities included as part of an operation to make a fuel product are incorporated into our energy and emission calculations. Activities related to building infrastructure — such as manufacturing plants, roads, and equipment — are not included. Contributions of infrastructure-related energy use and emissions to total WTW energy use and emissions are generally small.

Although the default version of the GREET model allows users to conduct single, point-based simulations (in which a single value is used for an input parameter), the new version of the GREET model — GREET 1.6 — is designed to allow users to also conduct stochastic simulations, in which the GREET model can generate energy and emission results with probability distribution functions. For the current study, stochastic simulations are conducted. To conduct such simulations with GREET 1.6, users need to have both Microsoft Excel® and Decisioneering’s Crystal Ball® software.

GREET 1.6 was developed to simulate light-duty vehicles. In order to simulate buses and farming tractors, the model was reconfigured using vehicle fuel economy and emission inputs for buses and farming tractors. For bus simulations, results are generated on a per-mile-driven basis, the same as for light-duty vehicles. For farming tractor simulations, results are generated on a per-hour-of-operation basis; thus energy use and emissions for farming tractors are determined per hour of operation. The per-mile and per-hour energy and emission data for buses and farming tractors are input into GREET.

The GREET model includes estimates of energy use, GHG emissions, and criteria pollutant emissions, as indicated below. This study addresses all of the following items.

1. Energy use
  - a. Total energy use (fossil and non fossil energy such as hydro-power and nuclear power)
  - b. Fossil energy use (petroleum, natural gas, and coal)
  - c. Petroleum use
  
2. GHG emissions (combined with global warming potentials [GWPs] to derive CO<sub>2</sub>-equivalent GHG emissions)
  - a. Carbon dioxide (CO<sub>2</sub>)
  - b. Methane (CH<sub>4</sub>)
  - c. Nitrous oxide (N<sub>2</sub>O)
  
3. Emissions of criteria pollutants (separated into total and urban emissions)
  - a. Volatile organic compounds (VOC)
  - b. Carbon monoxide (CO)
  - c. Nitrogen oxides (NO<sub>x</sub>)
  - d. Particulate matters (usually with diameter 10 microns or smaller, PM<sub>10</sub>)
  - e. Sulfur oxides (SO<sub>x</sub>)

Complete fuel-cycle energy impact analyses usually include total energy use, for which all energy sources — such as renewable energy and non-renewable energy (i.e., fossil energy) — are taken into account. Some analyses also address fossil energy impacts. In this case, fossil energy — including petroleum, natural gas, and coal — is taken into account. Because fossil energy resources are finite, analyses of fossil energy use reveal the impacts of energy resource depletion associated with a given vehicle/fuel system. This is especially important for ethanol; total energy impacts may not provide adequate information about it because the energy in ethanol comes from solar energy during crop growth, and use of solar energy per se for energy production is not a concern. Some studies also analyze petroleum displacement effects associated with vehicle/fuel systems. The petroleum displacement effect is an important issue for countries like the United States that rely on imported oil and intend to reduce that reliance.

The three GHGs are often combined together with their GWPs (Intergovernmental Panel on Climate Change [IPCC] 2001) to estimate CO<sub>2</sub>-equivalent GHG emissions. The GWPs of GHGs vary with the time horizon considered for determining them. With a time horizon of 100 years, GWPs are 1, 23, 296 for CO<sub>2</sub>, CH<sub>4</sub>, and N<sub>2</sub>O, respectively (IPCC 2001); these values were used in our study.

## Data Sources

GREET 1.6 contains input data regarding feedstock recovery, feedstock transportation, fuel production, and fuel transportation and distribution for both petroleum diesel and ethanol. Assumptions regarding petroleum diesel were reviewed and revised during a study that Argonne conducted for General Motors Corporation (General Motors Corporation et al. 2001a,b,c).

Assumptions regarding ethanol production pathways were first documented in Wang et al. (1997; 1999). During the current study, efforts were made to obtain new data on the energy use associated with fertilizer production, corn farming, and ethanol production and on N<sub>2</sub>O emissions



from agricultural soils. Revised assumptions for these activities are documented here. Assumptions regarding ethanol unchanged from the earlier studies can be found in Wang et al. (1997; 1999).

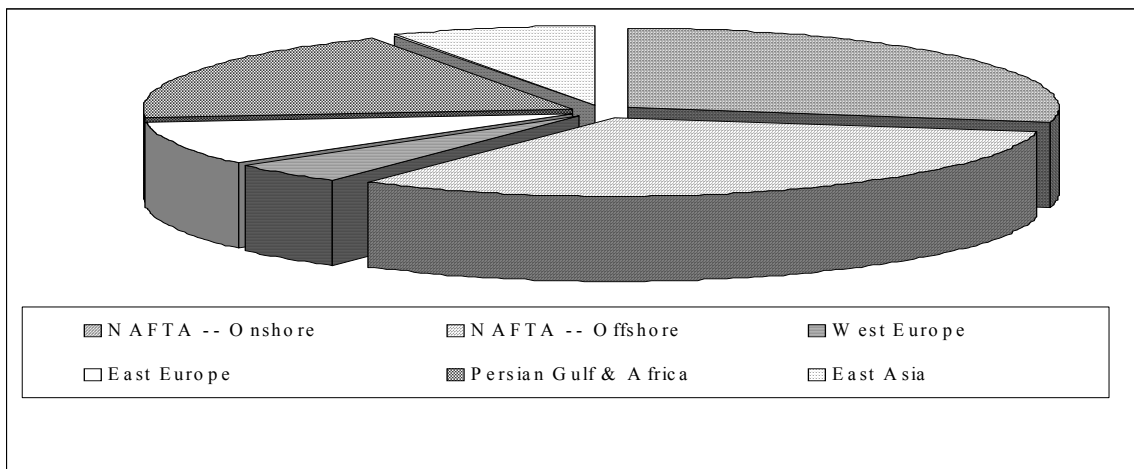
This study uses a probability-based simulation feature included in GREET 1.6. Probability-based parametric assumptions are required for these simulations, and wherever possible, were established for the key input parameters of this study.

## Fertilizer Production

### *Production and Consumption of Nitrogen Fertilizers*

Since 1999, the United States has become a net importer of nitrogen (N) fertilizer, as indicated by statistics from the Food and Agriculture Organization of the United Nations (1999). The increase in fertilizer imports is attributable to the abundant and relatively cheap new offshore sources, especially in the Commonwealth of Independent States, which have become available over the past decade. This development requires re-evaluation of GREET’s treatment of N-fertilizer production energy requirements by taking into account the shifts in fertilizer production between North America and production areas outside of North America.

Figure 2 presents the shares of U.S.-imported N-fertilizer by region for the period from July 2000 through June 2001. The chart was developed on the basis of data provided by the Economic Research Service of the U.S. Department of Agriculture (Taylor 2002). The chart reveals that NAFTA (North American Free Trade Association) onshore (Canada and Mexico) and NAFTA offshore (Central and South American countries) account for more than one half of the total tonnage of imported N-fertilizer products (a slate comprising anhydrous ammonia, aqua ammonia, nitrogen solutions, solute ammonium nitrate, and solid urea). The grand total of nitrogen product imports is just over 14.6 million short tons (Table 2, extracted from Taylor [2002]). Total U.S. N-fertilizer consumption (as products) is about 24.4 million tons (Taylor 2002) — making the United States a net importer of N-fertilizer products, with imports accounting for about 60% of the total N-fertilizer consumption.



**Figure 2.** Shares of U.S. Imported Nitrogen Fertilizer by Region (based on Taylor 2002)

**Table 2.** U.S. N-Fertilizer Import Source Nations and Amounts for July 2000 to June 9

2001<sup>a</sup>

Source Nation	Anhydrous Ammonia	Aqua Ammonia	Nitrogen Solutions	Ammonia Nitrate (solute)	Urea (solid)	Total	Share of Import (%)
<b>NAFTA Onshore</b>	<b>948,130</b>	<b>3,126</b>	<b>263,600</b>	<b>514,944</b>	<b>1,820,447</b>	<b>3,550,247</b>	<b>24.3</b>
Canada	901,481	3,126	263,600	514,944	1,820,412	3,503,563	24.0
Mexico	46,649				35	46,684	0.3
<b>NAFTA Offshore</b>	<b>3,491,997</b>		<b>3,054</b>	<b>847</b>	<b>538,542</b>	<b>4,034,440</b>	<b>27.6</b>
Trinidad & Tobago	3,228,091		3,054		389,214	3,620,359	24.8
Venezuela	173,167				74,140	247,307	1.7
Others	90,739			847	75,188	166,774	1.1
<b>West Europe</b>	<b>12,263</b>	<b>864</b>	<b>109,571</b>	<b>170,773</b>	<b>259,738</b>	<b>553,209</b>	<b>3.8</b>
Netherlands	12,263		48,250	100,843	82,804	244,160	1.7
Others		864	61,321	69,930	18,134	309,049	2.1
<b>East Europe</b>	<b>859,084</b>		<b>1,731,421</b>	<b>328,672</b>	<b>156,738</b>	<b>3,075,915</b>	<b>21.1</b>
Ukraine	516,733		405,424	150,359		1,072,516	7.3
Russia	253,866		563,518	96,171	10,484	924,039	6.3
Lithuania			362,600	19,937		382,537	2.6
Poland			161,144		36,033	197,177	1.4
Bulgaria			88,453	19,854	75,331	183,638	1.3
Others	88,485		150,282	42,351	34,890	316,008	2.2
<b>Persian Gulf and Africa</b>	<b>91,304</b>		<b>107,499</b>	<b>60,311</b>	<b>2,133,370</b>	<b>2,392,484</b>	<b>16.4</b>
Saudi Arabia	65,482		13,228		667,600	746,310	5.1
Qatar				222	442,245	442,467	3.0
Egypt				11,532	426,007	437,539	3.0
Bahrain				45	428,780	428,825	2.9
Others	25,822		94,271	48,512	168,738	337,343	2.3
<b>East Asia</b>	<b>226,322</b>	<b>1,008</b>	<b>23,133</b>	<b>515</b>	<b>752,948</b>	<b>1,003,926</b>	<b>6.9</b>
Indonesia	217,200				128,807	346,007	2.4
Malaysia	6,301		23,133		298,387	327,821	2.2
China				1	210,345	210,346	1.4
Others	2,821	1,008		514	115,409	119,752	0.8
<b>Total: products</b>	<b>5,629,100</b>	<b>4,998</b>	<b>2,238,278</b>	<b>1,076,062</b>	<b>5,661,783</b>	<b>14,610,221</b>	<b>100</b>
<b>Total: N nutrient</b>	<b>4,615,863</b>	<b>1,010</b>	<b>671,453</b>	<b>360,481</b>	<b>2,604,421</b>	<b>8,253,228</b>	

<sup>a</sup> Amounts are in short tons and are based on Taylor (2002).

Table 3 lists the consumption shares of major N-fertilizer types in the United States. As the table shows, there are eight types of N-fertilizer used on U.S. farms, but the three major types are anhydrous ammonia, nitrogen solutions, and urea. GREET, on the other hand, includes three fertilizer types for simulations: ammonia, urea, and ammonium nitrate. The eight types are combined into the three fertilizer types in the GREET model for our simulations (see footnote c to Table 3).

**Table 3.** U.S. Nitrogen Fertilizer Consumption for Calendar Year 2000<sup>a</sup>

<b>Fertilizer Type</b>	<b>Product Consumption<sup>b</sup></b>	<b>Nutrient Consumption</b>	<b>Share by Type (%)<sup>c</sup></b>
Anhydrous Ammonia	4,445,809	3,645,564	35.6
Aqua Ammonia	338,026	68,309	0.7
Nitrogen Solutions	10,424,279	3,127,142	30.5
Ammonium Nitrate	1,698,355	568,949	5.6
Urea	4,697,642	2,160,916	21.1
Ammonium Sulfate	1,121,318	213,947	2.1
Ammonium Thiosulfate	356,031	60,621	0.6
Other	1,346,600	403,980	3.9
<b>Total</b>	<b>24,428,060</b>	<b>10,249,430</b>	<b>100.0</b>

<sup>a</sup> Amounts are in short tons.

<sup>b</sup> From Association of American Plant Food Control Officials (AAPFCO) and The Fertilizer Institute (2001).

<sup>c</sup> The shares are based on nitrogen nutrient consumption. While there are eight types of N-fertilizer that are used on U.S. farms, the GREET model has energy and emission simulations for three types: ammonia, urea, and ammonium nitrate. For GREET simulations, the shares of anhydrous ammonia, aqua ammonia, nitrogen solutions, and other are combined together as the share of ammonia (70.7%), and the shares of ammonium nitrate, ammonium sulfate, and ammonium thiosulfate are combined together as the share of ammonium nitrate (8.3%).

#### *Feedstock Use, Energy Use, and Emissions for Fertilizer Production*

In our analysis, we include estimates of energy use and emissions of nitrogen, phosphate, and potassium fertilizers — the three major fertilizer types used for corn farming. Among the three types, nitrogen fertilizer is used most intensively for corn farming, and it is the most energy intensive one to produce.

Our estimates of feedstock and process fuel use during the production of ammonia, urea, ammonium nitrate, and phosphoric acid are discussed in Appendix A and summarized in Table 4. On the basis of the results presented in Appendix A, we developed two cases (low energy use and high energy use) for production of ammonia, urea, nitric acid, and phosphoric acid (Table 4). The two cases are derived primarily from reports prepared by the U.S. Department of Energy (DOE) and The Fertilizer Institute (TFI) (DOE 2000; TFI 2001). The European Fertilizer Manufacturers Association (EFMA) also reports energy use and emissions associated with fertilizer production (EFMA 1995; 2000a, b, c, d). DOE's total fuel use value is close to that reported by EFMA (no data for shares of process fuels and electricity are available from EFMA), and thus no separate estimate is developed from the EFMA data. For production of phosphoric acid, TFI and EFMA data are averaged because of their similarity.

The GREET model estimates energy use and emissions associated with transporting fertilizers and feedstocks from their origin to their destination by specifying transportation logistics such as transportation distance and transportation mode. The GREET estimated energy use for transporting fertilizer from plants to farms is about 274 Btu per lb of fertilizer.

**Table 4.** Summary of Feedstock Use, Energy Use, and Emissions for Fertilizer Production (based on results presented in Appendix A)

		Ammonia (NH <sub>3</sub> )		Urea		Nitric Acid (HNO <sub>3</sub> )		Ammonium Nitrate	Sulfuric Acid (H <sub>2</sub> SO <sub>4</sub> )	Phosphoric Rock	Phosphoric Acid	
		Low	High	Low	High	Low	High				Low	High
Feedstock (tons/ton product)	Natural Gas	0.46	0.46									
	NH <sub>3</sub>			0.567	0.567	0.405	0.405	0.213				
	HNO <sub>3</sub>							0.788				
	H <sub>2</sub> SO <sub>4</sub>										2.674	2.674
	Phos. rock										3.525	3.525
Process fuel <sup>a</sup> (mmBtu/ton)	Electricity	1.838	0.389	0.212	0.046	0.006	0.006	0.242	0.0635	0.245	0.557	0.371
	Other fuels <sup>b</sup>	3.556	11.371	1.464	2.816	0.526	0.526	0.440	0.0445	0.000	1.546	6.800
	Total	5.394	11.760	1.676	2.862	0.532	0.532	0.682	0.108	0.245	2.103	7.171
Total energy (mmBtu/ton)	Electricity	1.838	0.389								0.557	0.371
	Other fuels	3.556	11.371								1.546	6.800
	Energy in feedstock	18.906	18.906								1.160	1.160
	Total	24.300	30.666								3.263	8.331
Process emissions <sup>c</sup> (g/ton)	VOC	4,285.8	4,285.8									
	CO	27,240	7,173.2									
	NO <sub>x</sub>					549.34	998.80					
	PM <sub>10</sub>			53.118	147.55			1,058.3				
	SO <sub>x</sub>	9.08	26.332						18,160			
	N <sub>2</sub> O					1,648	14,183					

<sup>a</sup> These values represent process fuel use for the individual process only. All values for energy calculations in this study are based on lower heating values (LHVs) of fuels.

<sup>b</sup> Mainly natural gas.

<sup>c</sup> These values are emissions in addition to the emissions associated from combustion of process fuels. CO<sub>2</sub> emissions for fertilizer manufacture are calculated by using a mass balance approach inside the GREET model; the difference in carbon between input items and output products becomes CO<sub>2</sub> emissions.

**Table 5.** Parametric Assumptions for Fertilizer Production in the GREET Model (per ton of product, based on Table 4)

	Ammonia			Nitric Acid			Urea			Ammonium Nitrate	Sulf. Acid	Phosp. Rock	Phosphoric Acid		
	Low	Mean	High	Low	Mean	High	Low	Mean	High				Low	Mean	High
Total energy input (mmBtu) <sup>a</sup>	24.30	27.49	30.67		0.532		1.676	2.269	2.862	0.682	0.108	0.245	2.103	4.637	7.171
Total NG input (mmBtu) <sup>b</sup>	22.46	26.37	30.28		0.526		1.464	2.140	2.816	0.440	0.0445	0.000	1.546	4.173	6.800
Electricity input (mmBtu) <sup>c</sup>	1.84	1.12	0.39		0.006		0.212	0.129	0.046	0.242	0.0635	0.245	0.557	0.464	0.371
NG process fuel input (mmBtu)	3.55 <sup>d</sup>	7.46 <sup>d</sup>	11.37 <sup>d</sup>		0.526		1.464	2.140	2.816	0.440	0.0445	0.000	1.546	4.173	6.800
NG process fuel share of total NG energy input (%)	15.8	28.3	37.5		100		100	100	100	100	100		100	100	100
Ammonia (tons)					0.405			0.567		0.213					
Nitric acid (tons)										0.788					
Sulfuric acid (tons)														2.674	
Phosphoric rock (tons)														3.525	
Processing emissions (g)															
VOC		4,286													
CO	27,240	3600.2	7,173												
NO <sub>x</sub>				549.3	774.1	998.8									
PM <sub>10</sub>							53.118	100.33	147.55	1,058.3					
SO <sub>x</sub>		26.33									18,160				
N <sub>2</sub> O				1,648	7,916	14,183									

<sup>a</sup> The total energy input here includes energy in feedstocks and in process fuels.

<sup>b</sup> Although some other process fuels besides NG are used in fertilizer plants, we assume here that all process fuels are NG.

<sup>c</sup> Electricity input here is calculated as the difference between the total energy input and the NG input. Energy losses during electricity generation are not included in this table. They are taken into account inside the GREET model and in the final energy and emission results for ethanol.

<sup>d</sup> NG input as the process fuel for ammonia production is calculated from total NG input subtracted by NG input as feedstock for ammonia production (0.46 tons of NG, or 18.91 mmBtu, of NG per ton of ammonia).

## Corn Farming

Shapouri et al. of the U.S. Department of Agriculture (USDA) (Shapouri et al. 2002) recently developed updated estimates of the energy requirements for corn farming. They used data from the 1996 Agricultural Resource Management Survey (formerly the Farm Costs and Returns Survey) to determine corn farming energy use and chemical application. The data were for nine key Midwest corn-producing states that produce 80% of total U.S. corn. Table 6 presents energy and chemical use values from Shapouri et al. that are used in GREET simulations in this study. Of the total farming energy use, 46% is from diesel fuels, 20% from gasoline, 15% from liquefied petroleum gas (LPG), 12% from NG, and 6% from electricity. These energy sources power tractors, irrigation equipment, crop-drying machinery on corn farms, and other activities.

**Table 6.** Corn Farming Energy and Chemicals Use (per bushel of corn produced)

	Minimum <sup>a</sup>	Mean <sup>a</sup>	Maximum <sup>a</sup>
Farming Energy (Btu, LHV) <sup>b</sup>	19,963	23,288	34,224
Share of Farming Energy by Fuel Type (%)			
Diesel		38.3	
Gasoline		12.3	
LPG		18.8	
NG		21.5	
Electricity		9.0	
N fertilizer: N (g)	305	470	577
P fertilizer: P <sub>2</sub> O <sub>5</sub> (g)	88	175	273
K fertilizer: K <sub>2</sub> O (g)	18	215	391

<sup>a</sup> The minimum and maximum values are based on the range of the results of the nine Midwestern states (Illinois, Indiana, Iowa, Minnesota, Nebraska, Ohio, Michigan, South Dakota, and Wisconsin). The mean values are the nine-state average values.

<sup>b</sup> The farming energy use values presented in Shapouri et al. are in higher heating values (HHVs). The values presented here are the LHV values that were used in this study. The farming energy values here include use of diesel fuel, gasoline, LPG, NG, electricity, custom work, lime, and seeds.

In addition to the energy use rates presented in Table 6, about 6,000 Btu of energy is consumed to transport each bushel of corn from farms to ethanol plants. This value is calculated inside GREET as a function of truck fuel economy, truck payload, and transportation distance.

Besides the three fertilizer types listed in Table 6, our analysis includes energy and emissions associated with the manufacture of herbicides and insecticides (see Wang et al. 1997).

## **Nitrous Oxide Emissions from Nitrogen Fertilizer Applications in Corn Fields**

Appendix B documents our efforts to obtain new data on cornfield N<sub>2</sub>O emissions. On the basis of data presented there and considering the potential N-fertilizer-induced N<sub>2</sub>O emissions outside of growing seasons and a small increase in indirect N<sub>2</sub>O emissions from nitrate, we have increased N<sub>2</sub>O emissions for our new “point estimate” from 1.5% to 2.0%, with a range of 1% to 3%.

## **Ethanol Production**

Both wet and dry milling ethanol plants produce fuel ethanol in the United States. As of December 2002, the U.S. total ethanol production capacity is about 2.704 billion gal/yr. Of this, 1.108 billion gal are produced in wet mill plants, the rest in dry mill plants (Shaw 2002). That is, wet mill plants account for about 41% of the total capacity, with the remaining 59% being dry mill capacity. The large share of dry milling capacity results from the fact that recently built ethanol plants are all dry mills — a trend that will continue in the future because dry mills can be smaller and require less capital investment than wet mills and because co-products (such as glucose from wet mills) are not bringing returns commensurate with production costs. Thus, we assume that by 2010 — the target year for our analysis — 70% of total U.S. ethanol production will be in dry mills, and the remaining 30% will be in wet mills.

The USDA study (Shapouri et al. 2002) surveyed ethanol plants to determine their energy use. Revised energy use values for ethanol production have been estimated for GREET. They are as follows, based on the USDA survey results: 36,119 Btu/gal (LHV) of ethanol for dry mills (89.7% of which is energy provided by NG and coal, and the remaining 10.3% is energy provided by electricity), and 45,954 Btu/gal (LHV) for wet mills (all provided by NG and coal). Note that Shapouri et al. report HHVs in all cases, while GREET uses LHVs for simulations.

The GREET model estimates energy use and emissions associated with transporting ethanol from ethanol plants to fuel refueling stations by specifying transportation logistics such as transportation distance and transportation mode. The GREET-estimated energy use for transporting ethanol from plants to refueling stations is about 1,480 Btu/gal of ethanol.

## **Additive Production**

Several manufacturers of chemical solvents and blending agents supply the additive needed to combine diesel fuel with ethanol in a manner that precludes blend instability or separation of the two components. Early E-diesel blends used co-solvent additives of up to 5% by volume, but more recently, the “treat rate” for co-solvents has been closer to 1% to 2%. We contacted several additive suppliers that are currently active in E-diesel blending to obtain insights regarding the production energy requirements and energy density per unit volume of their products. All of those who responded agreed on two points:

- (1) The heating value of one or more of the available E-diesel additives is approximately equal to that of conventional gasoline.

- (2) Process energy for additive manufacture is supplied by NG and grid electricity at rates (energy consumption and GHG generation per output Btu) that are comparable to those for the products of a state-of-the-art petroleum refinery.

Specific responses to questions about energy balances were graciously supplied by two additive manufacturers. We examined the information provided by the two additive manufacturers and determined that there could be significant variation in production processes for additives. We believe that additives can be produced along two general pathways: one in petroleum refineries where they are produced as a co-product with other refinery products, and the other in a chemical plant where they are produced as one of the designated products. For the petroleum refinery pathway, we assumed an energy efficiency of 85% for additive production — the efficiency for gasoline production applied in GREET. For the chemical plant pathway, we assumed an energy efficiency of 68%. This efficiency is consistent with the efficiency of many chemical processes, such as production of methanol, dimethyl ether, and hydrogen. In GREET simulations, we applied a distribution function with minimum, average, and maximum efficiencies of 68%, 76.5%, and 85%, respectively. We acknowledge, based on data provided by manufacturers, that the current batch production process for the chemical plant pathway could have an efficiency as low as 50%. However, if E-diesel is ever to have any significant market share, additive production will be likely to move from batch to continuous production; otherwise, cost-competitiveness for the finished fuel will be very unlikely.

On the basis of information provided by additive manufacturers, we used a product density of 7.5 lb/gal for additives and a heating value comparable to that of gasoline (approximately 115,000 Btu/gal). We further applied a process fuel split (of 80% NG, 20% electricity) in GREET simulations.

## **Energy Use and Emissions of Buses and Farming Tractors**

E-diesel stakeholders generally agree that the near- and medium-term thrust for introducing E-diesel into the fuel market will target (1) agricultural equipment in grain-growing regions, and (2) transit buses in central and western urban areas that are currently designated as nonattainment areas for ambient ozone or, when designated, for fine particulate standards. An ED10 (10% ethanol) product containing, on average, 1% co-solvent additive (by volume) can fuel agricultural equipment and, to a lesser extent, the medium and light heavy-duty farm trucks. Transit buses will be fueled by an ED15 (15% ethanol, 1.5% additive) blend because the higher ethanol content has been associated with improved effectiveness in reducing combustion-related fine particle emissions — a major urban health problem. Our purpose is to identify criteria pollutant and CO<sub>2</sub> emission rates currently associated with these vehicle classes and express them as (or enable their conversion to) units consistent with the GREET methodology.

### *Agricultural Tractors and Trucks*

A testing program using an ED10 blend to fuel agricultural tractors is underway through a cooperative agreement among the State of Illinois, the University of Illinois at Urbana-Champaign, members of the E-diesel Consortium, and John Deere, Inc. (Hansen et al. 2001).



Thus, performance data are being developed using John Deere agricultural equipment, and we have applied information specific to this equipment (from the John Deere web site) in our calculations.

For Deere tractors, the fuel consumption rate at rated engine speed (rpm) appears to be an approximately monotonic function of rated horsepower, regardless of whether the tractor is two-wheel drive (2WD) or four-wheel drive (4WD) (Table 7). Utility tractors start at about 50 hp, and the largest agricultural tractors are rated at 450 hp. We selected a value of 365 hp, corresponding to the midpoint of 4WD units but incorporating both top 2WD units and maximum 4WD unit power requirements if a 70-hp variation (plus or minus) about this midpoint is assumed.

**Table 7.** Fuel Consumption Rates and Power Output of John Deere Tractors<sup>a</sup>

Tractor Type	Power Output	
	mmBtu/hr	hp-h/mmBtu
<b>2WD Tractors</b>		
<i>5320 Utility Tractor: 55 hp</i>		
Power takeoff at 2,400 rpm	0.440	126.66
Maximum power takeoff at 1,900 rpm	0.410	142.53
<i>6310 Tractor: 80 hp</i>		
Power takeoff at 2,300 rpm	0.655	124.48
Standard power takeoff at 2,200 rpm	0.640	128.37
Maximum engine power at 1,900 rpm	0.630	140.04
<i>7610 Tractor: 120 hp</i>		
Power takeoff at 2,100 rpm	0.915	132.10
Standard power takeoff at 2,100 rpm	0.915	132.10
Maximum engine power at 2,100 rpm	0.900	140.66
<i>8420 Tractor: 235 hp</i>		
Power takeoff at 2,200 rpm	1.695	139.65
Standard power takeoff at 2,200 rpm	1.695	139.65
Maximum power takeoff at 2,000 rpm	1.850	148.13
Maximum engine power at 2,199 rpm	1.685	120.67
<b>4WD Tractors</b>		
<i>9200 Tractor: 310 hp</i>		
Power takeoff at 2,100 rpm	1.970	134.83
Standard power takeoff at 1,900 rpm	2.085	142.61
Maximum power takeoff at 1,900 rpm	2.085	142.45
Maximum engine power at 2,097 rpm	1.985	124.09
<i>9400 Tractor: 425 hp</i>		
Power takeoff at 2,100 rpm	2.210	141.21
Standard power takeoff at 1,900 rpm	2.315	148.21
Maximum power takeoff at 1,900 rpm	2.315	148.21
Maximum engine power at 2,101 rpm	2.605	132.34

<sup>a</sup> From <http://products.deere.com/webapp/commerce/command/CategoryDisplay?path=FR&cgnbr=Tractors> (accessed 8/29/02). For diesel fuels, 1 mmBtu is equal to 7.78 gal of CD.

While fuel consumption rate increases monotonically for these tractors, specific power output per mmBtu of fuel used at rated speed (rpm) is remarkably uniform, as shown in Table 7.

EPA's 1991 off-road emissions study (EPA 1991) assigned emission factors in g/hp-h and lb/1,000 gal of diesel fuel to agricultural tractor operation. Corresponding pollutant values are listed in Table 8.

**Table 8.** Emissions from Agricultural Tractors<sup>a</sup>

Pollutant	Emissions	
	g/hp-hr	lb/1,000 gal of diesel
HC	1.59	63.55
CO	4.47	174.9
NO <sub>x</sub>	11.19	438.6
PM <sub>10</sub>	1.17	45.7
SO <sub>x</sub>	0.80	31.2

<sup>a</sup> Based on EPA (1991); the values listed incorporate a specific power factor of about 138 hp-hr/mmBtu.

**Table 9.** Emissions Factors with the Estimated Fuel Consumption

Pollutant	Emissions	
	g/hr	g/mmBtu
HC	580	265
CO	1,630	745
NO <sub>x</sub>	4,085	1,865
PM <sub>10</sub>	430	195
SO <sub>x</sub>	290	130

control tier (based on current and future standards) generally corresponds to a control technology set. Tractors are already under Tier 1 control (see Table 10), and Tier 2 begins next year. The current tractor fleet age distribution is approximately 60% base, 30% Tier 0, and 10% Tier 1. In the long term, the fleet will be covered 100% by Tier 2 and Tier 3. Under Tier 3, tractors cannot use 3,000-ppm-S diesel fuel. We assumed 350-ppm-S diesel for Tier 2 and Tier 3 nonroad vehicles.

To perform CO<sub>2</sub> calculations, it is necessary to apply the fuel consumption (FC) relationship (expressed in gal), as calculated across the spectrum of Deere tractors, i.e.,  $FC/hr = 0.0413 \text{ hp} + 2.09$  ( $r^2 = 0.96$ ). For the 365-hp tractor, this translates to 17.1 gal of diesel fuel (or 2.19 mmBtu) per hour. The tractor power range covering 70 hp to either side of the 365 hp yields a fuel consumption range between 14 and 20 gal/hr. Applying EPA factors to convert from mmBtu to hours gives the approximate (rounded to the nearest 5) midpoint emission factors listed in Table 9 (g/hr, g/mmBtu).

EPA estimates that agricultural tractors operate about 411 hrs/yr (90% of that occurs from March to October) — meaning our average tractor consumes about 7,030 gal (905 mmBtu) of diesel per year and, according to the *Nonroad Engine and Vehicle Emission Study* (EPA 1991), emits 1,690 kg NO<sub>x</sub>, 240 kg hydrocarbons (HC), 675 kg CO, 175 kg PM<sub>10</sub>, and 120 kg SO<sub>x</sub> per year (about 95% during the 6–8 month growing season).

EPA’s NONROAD model (EPA 2002a) is still officially in draft form (not approved for state implementation plan submissions), but it provides significantly updated rates, based on emission control technology level, for diesel agricultural tractors relative to the 1991 values. In this case, each emission

**Table 10.** Criteria Pollutant Emissions from Nonroad Tractors in g/hp-hr

<b>Pollutant</b>	<b>Base Rate</b>	<b>Tier 0</b>	<b>Tier 1</b>	<b>Tier 2</b>	<b>Tier 3 (after 2007)</b>
THC	1.42	0.60	0.319	0.32	0.16
CO	1.88	1.13	0.52	0.52	0.52
NO <sub>x</sub>	11.10	8.38	5.452	3.76	2.35
PM <sub>10</sub>	0.82	0.25	0.156	0.10	0.10

Based on the relatively constant conversion factor 18 hp-hr/gal of diesel fuels, we converted these rates into g/mmBtu (Table 11).

**Table 11.** Criteria Pollutant Emissions from Nonroad Tractors in g/mmBtu

<b>Pollutant</b>	<b>Base Rate</b>	<b>Tier 0</b>	<b>Tier 1</b>	<b>Tier 2</b>	<b>Tier 3 (after 2007)</b>
THC	200	84	45	45	22
CO	260	160	72	72	72
NO <sub>x</sub>	1,550	1,170	760	525	330
PM <sub>10</sub>	115	35	22	14	14

We have assumed that tractors fueled by ED10 in a future of widespread use will comply with Tier 2 standards, with a very small proportion (1.5%) that are Tier 3 compliant. This level of stringency will, on average, not require (but can accept) the use of low-sulfur (15-ppm) diesel.

In heavy-duty truck tests conducted by Southwest Research Institute (SwRI) for Archer Daniels Midland (ADM) (Marek and Evanoff 2001), two 1999 model year Mack E-7 units were tested (see Marek and Evanoff 2001). The ED10 experienced a net 7% loss in fuel economy (by fuel volume) relative to diesel fuel, while ED15 experienced a 10% loss. PM emissions were down in both cases by at least 20%, and these are recent-technology engines. NO<sub>x</sub> emissions were about the same.

ED10 emissions testing was also performed by the Colorado School of Mines for AAE/Octel-Starreon on a 1991 DDC Series 60 (Peeples and MacMillan 2001). The researchers reported a small (2% to 5%) net NO<sub>x</sub> reduction — which is lost in the noise because some rpm/load combinations actually increased NO<sub>x</sub> (a finding duplicated during Volkswagen engine testing by Automotive Testing Laboratory and Argonne National Laboratory [Cole et al. 2000]), as well as a 20% to 25% CO reduction and a 25% PM reduction (when looking at the actual representative segments of the engine map on which the unit was tested).

Based on the above considerations, for ED10 in agricultural tractor applications, we applied emission rates that correspond to the assumed changes relative to conventional diesel, as listed in Table 12.

**Table 12.** Fuel Consumption (mmBtu/hr) and Emissions (g/mmBtu) of Agricultural Tractors Fueled by Conventional Diesel, ED10, and ED15

	<b>Conventional Diesel</b>	<b>Relative Change of ED10, ED15 (%)</b>	<b>ED10</b>	<b>ED15</b>
Fuel Use (mmBtu/hr)	2.19	0.5, 4	2.2	2.27
Emissions (g/mmBtu)				
VOC	45	5, 7.5	46.5	47.6
CO	72	-10, -15	64.8	61.2
NO <sub>x</sub>	525	0, 2	525	535.5
PM <sub>10</sub>	14	-20, -25	11.2	10.5
N <sub>2</sub> O	0.92	5, 7.5	0.96	0.99
CH <sub>4</sub>	0.63	5, 7.5	0.66	0.68

*Transit Buses on E-Diesel Blends*

There is very little information about consistent, controlled tests of buses using E-diesel. One source is the testing conducted at Automotive Testing Laboratory and overseen by Argonne on the Volkswagen turbocharged direct-injection diesel light-duty engine (Cole et al. 2000). Also, the Chicago Transit Authority, in conjunction with SwRI, has conducted limited testing on buses fueled by ED15 (Marek and Evanoff 2001). These experiments showed no net fuel efficiency loss for an E-diesel blend relative to premium diesel (which may have a lower heating value than diesel #2).

Based on the limited results from Cole et al. (2000), we used the following modifications to standard diesel transit bus emission rates in MOBILE6 (Table 13), the latest version of EPA's MOBILE model for estimating vehicle emission factors (EPA 2002b).

**Table 13.** Baseline Bus Emission Rates and ED-Fueled Bus Emission Changes

	<b>Near-term (300-ppm-S diesel) buses</b>	<b>Long-term<sup>a</sup> (15-ppm-S diesel) buses</b>	<b>Changes by buses with ED10, ED15 (%)</b>	<b>Buses with ED10</b>	<b>Buses with ED15</b>
Btu content: Btu/gal	128,500	128,500	NA	123,120	120,430
Fuel economy (mi/volumetric gal)	3.73	3.73	-6, -10	3.51	3.36
Fuel economy (mi/gasoline-equiv. gal)	3.35	3.35	-2, -4	3.28	3.22
<b>Emissions (g/mi)</b>					
VOC	0.57	0.488	5, 7.5	0.513	0.525
CO	7.8	4.75	-10, -15	4.28	4.04
NO <sub>x</sub>	23	13.24	0, 2	13.24	13.5
PM <sub>10</sub>	0.34	0.217	-20, -25	0.174	0.163
N <sub>2</sub> O		0.01	0	0.01	0.01
CH <sub>4</sub>		0.007	0	0.007	0.007

<sup>a</sup> Long-term baseline bus emissions are estimated by using EPA's MOBILE6 except for N<sub>2</sub>O and CH<sub>4</sub>, which are GREET-based estimates.

Our decision regarding appropriate modifications to fuel consumption rates was not so straightforward. The limited testing on ED15 by the Chicago Transit Authority, in conjunction with SwRI, showed no statistically identifiable net fuel efficiency difference for an E-diesel blend relative to premium diesel. However, during the experiment E-diesel-fueled buses and the control neat diesel-fueled buses did not run the same routes under the same conditions because the test's purpose was simply to establish the viability of using ED15 in regular mass transit service. In fact, the 15 ED blend-fueled buses collectively accumulated 75,000 fewer service miles over the test period than their 15 control counterparts. The SwRI tests with the two Mack trucks were somewhat better controlled statistically and enabled a more legitimate "apples-to-apples" comparison of performance, even though the driving schedules and patterns were arguably not representative of transit buses. (Of course, this raises the question of whether transit bus operations in Chicago are representative of those of transit fleets in other cities that may one day use E-diesel.) We decided to adopt the SwRI heavy-duty results for ED15 as a defensible (if conservative) indicator for heavy-duty operations on ED15 generally. As shown in Table 13, we assigned a 10% volumetric fuel economy penalty to ED15/low-sulfur diesel blends relative to straight low-sulfur diesel.

We note that test results for tractors and buses using diesel and E-diesel are very limited. In fact, there were no controlled tests that assured that diesel and E-diesel would be tested in typical operating conditions for tractors or buses.

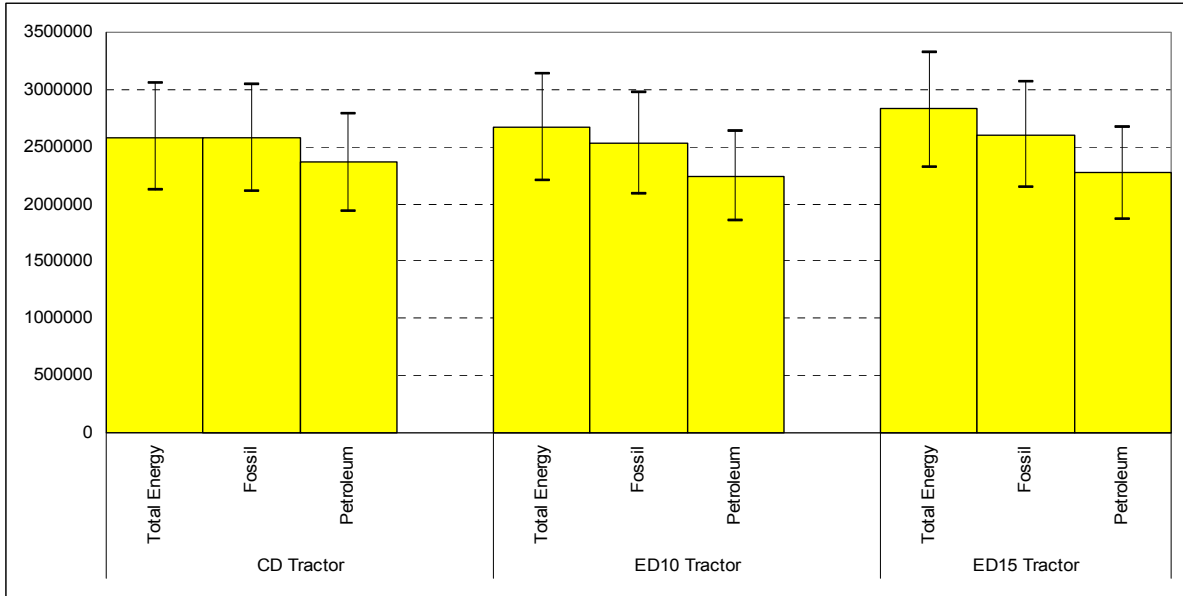
## Results

Figures 3 through 5 (covering model outputs) and 6 through 8 (covering case-to-case comparisons) present some key results of the GREET analysis. In each figure, the bars represent mean values, and the lines superimposed on the bars represent uncertainty ranges. As shown in Figures 3a and 3b, the spread in energy consumption rates in Btu/hr (tractor) or Btu/mi (bus) is largely a function of the range of representative hourly or per-mile fuel consumption rate (midpoint value plus or minus 18% for the tractor and 10% for the urban bus).

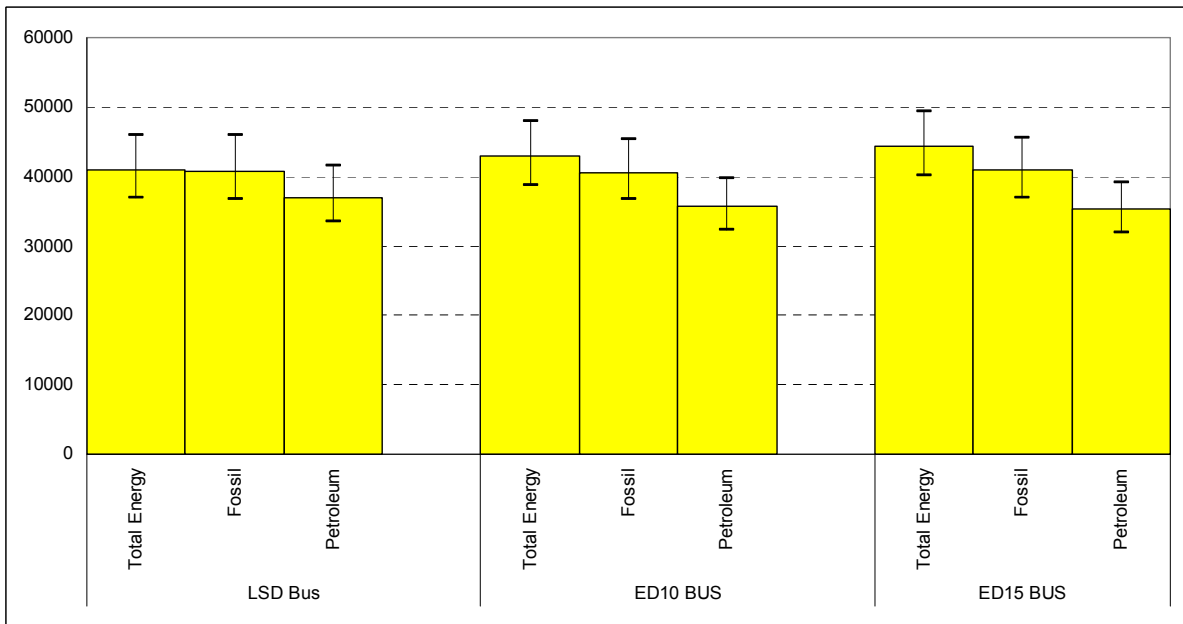
Not surprisingly, the fossil and petroleum shares decline across the fuels as an approximate function of percentage of ethanol, but not as dramatically as would be the case if ethanol mills and farming operations were powered predominantly by non-fossil fuels. In the case of global warming precursors (Figures 4a and 4b), total (GWP-weighted) fuel-to-fuel relationships in GHG emission rates are comparable for all cases, but the GHG/CO<sub>2</sub> ratio is slightly higher for the

E-diesel fuels because of higher N<sub>2</sub>O and methane concentrations in the WTP component for ethanol. Because fine-PM emissions are a concern in urban areas, we note in Figures 5a and 5b that the urban component of such emissions, while negligible for tractors, displays a very slight advantage for buses fueled by E-diesel over petroleum diesel counterparts, but the magnitude is probably not sufficient to drive fuel-oriented urban emission control policy decisions. Also note that total (i.e., urban and rural) fine-PM emissions are greater with the E-fuels because of their greater reliance on coal (upstream) as power plant fuel and process fuel.

Although use of E-diesel can achieve reductions in petroleum use (Figure 6a), the energy- and GHG-related net changes relative to use of conventional diesel (tractor) and low-sulfur diesel (bus) respectively, as shown in Figures 6a and 6b, do not establish a conclusive case for the superiority of E-diesel fuels. Within the range of our assumptions, as modeled within the 10% and 90% extreme values, it is possible that both ED10 and ED15 could produce greater overall emissions and consume more total energy and fossil fuels per unit of activity than neat diesel. Our analysis also shows that E-diesel fuels are likely to require more total energy input per unit of output heating value than either conventional or low-sulfur diesel. On the other hand, despite a relatively weak overall performance on *total* criteria pollutant emissions (Figure 7), buses fueled by E-diesel, do show a net reduction in important pollutants (PM<sub>10</sub> and CO) in urban areas (Figure 8). They are essentially neutral on VOCs as well as on NO<sub>x</sub> and SO<sub>x</sub> (VOC emission rates per unit of travel by diesels are so small to begin with that percentage changes less than 100% or so are inconsequential). Thus, the combined net benefit of petroleum displacement and reduction in urban fine particulate loading is possibly an attractive environmental and energy policy-oriented feature of E-diesel fuels.



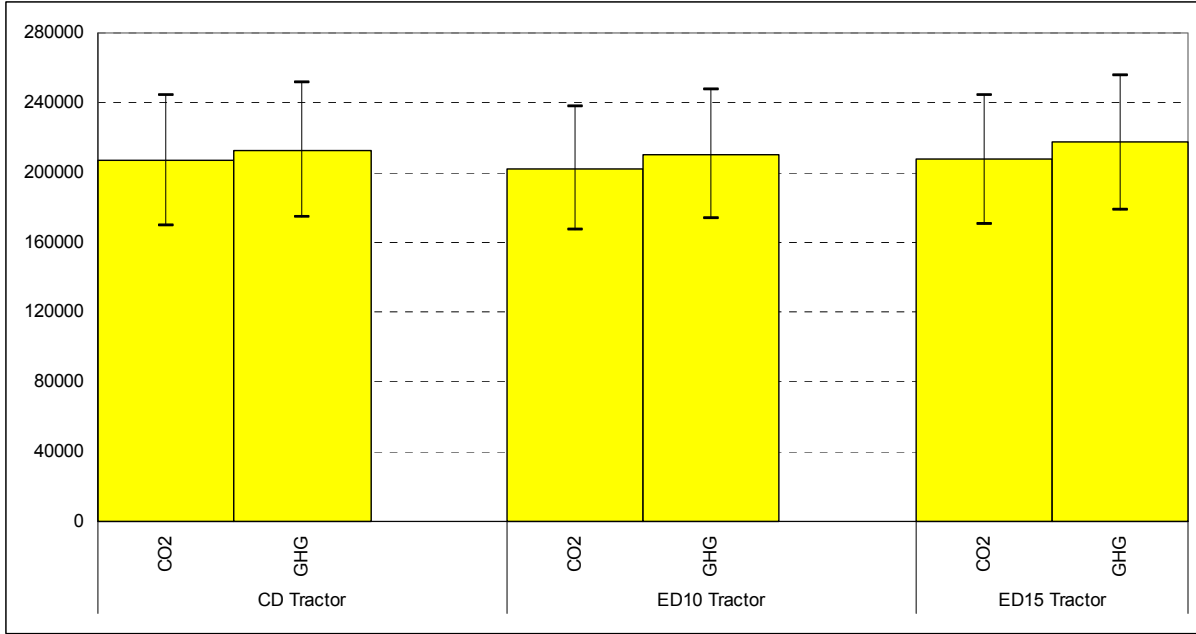
(a) Farming Tractors (Btu/hr)



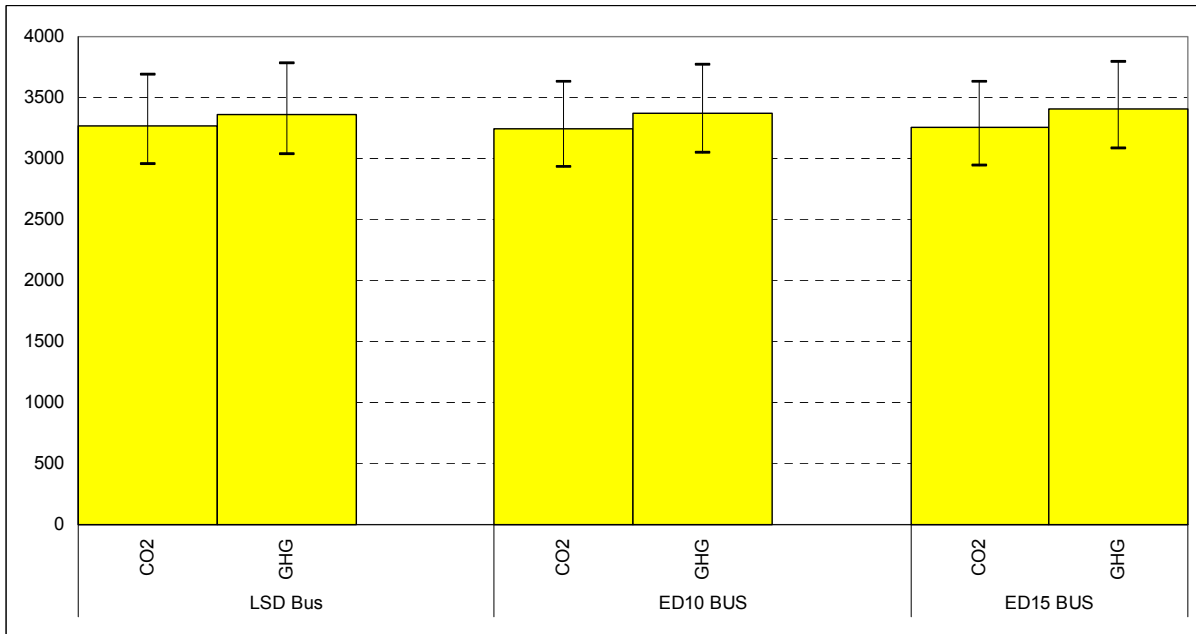
(b) Urban Buses (Btu/mi)

**Figure 3.** Well-to-Wheels Energy Use of Farming Tractors and Urban Buses



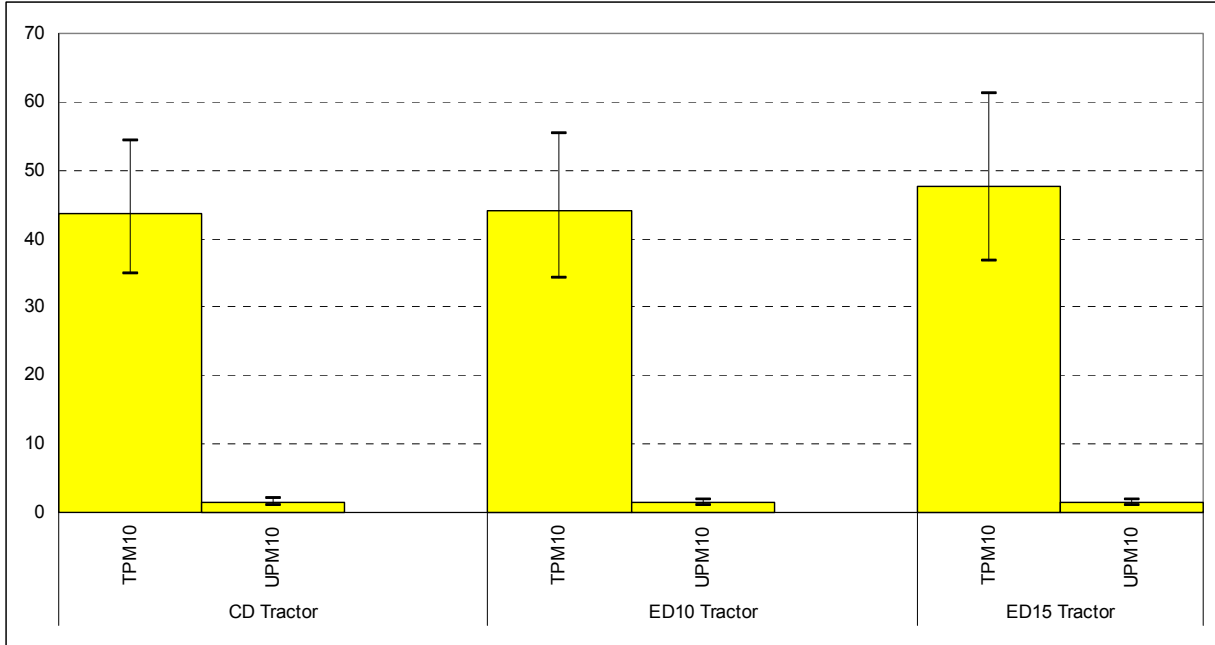


(a) Farming Tractors (g/hh)

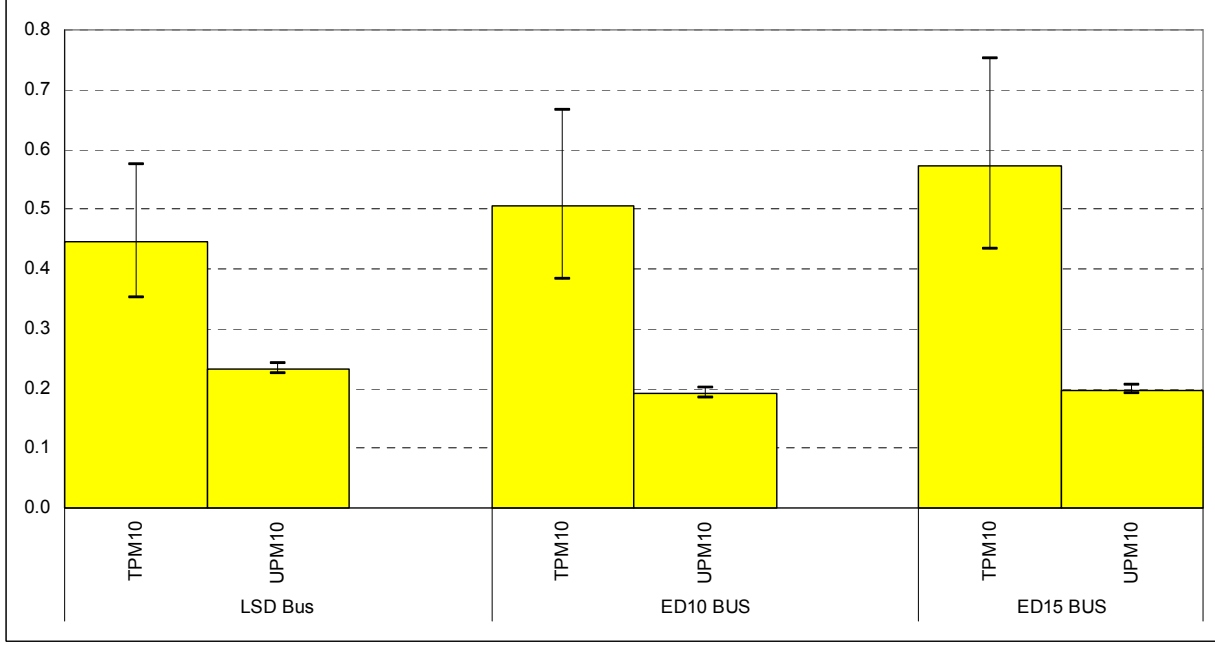


(b) Urban Buses (g/mi)

**Figure 4.** Well-to-Wheels CO<sub>2</sub>-Equivalent GHG Emissions of Farming Tractors and Urban Buses

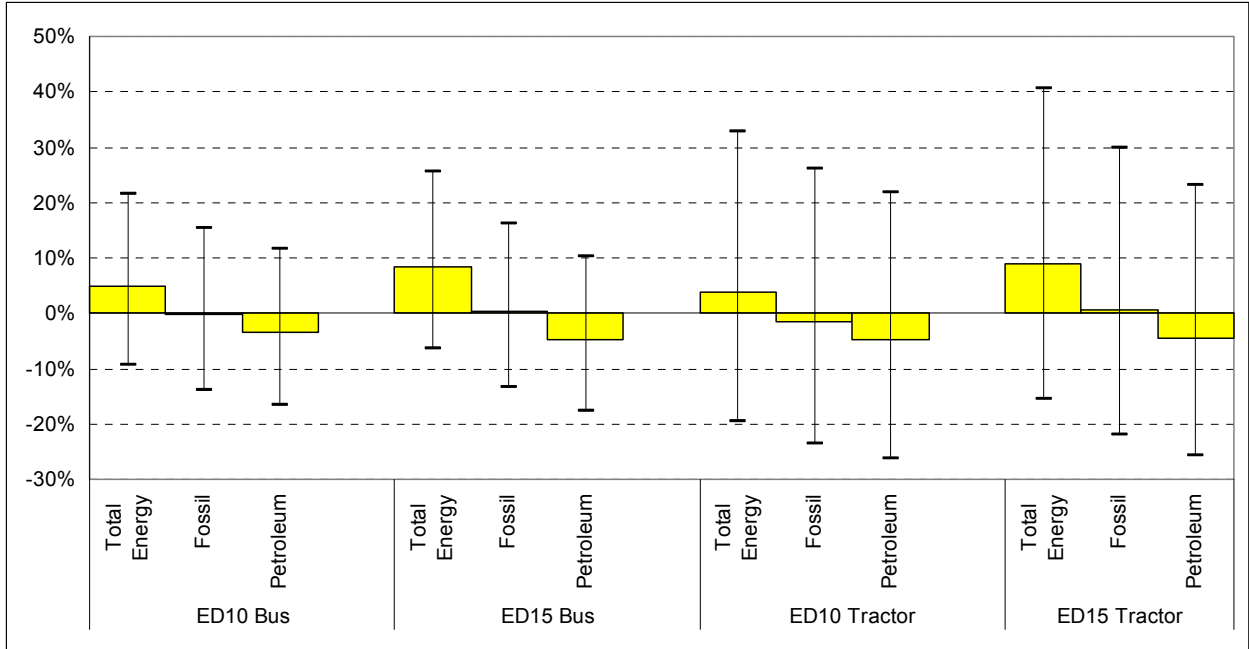


(a) Farming Tractors (g/hr)

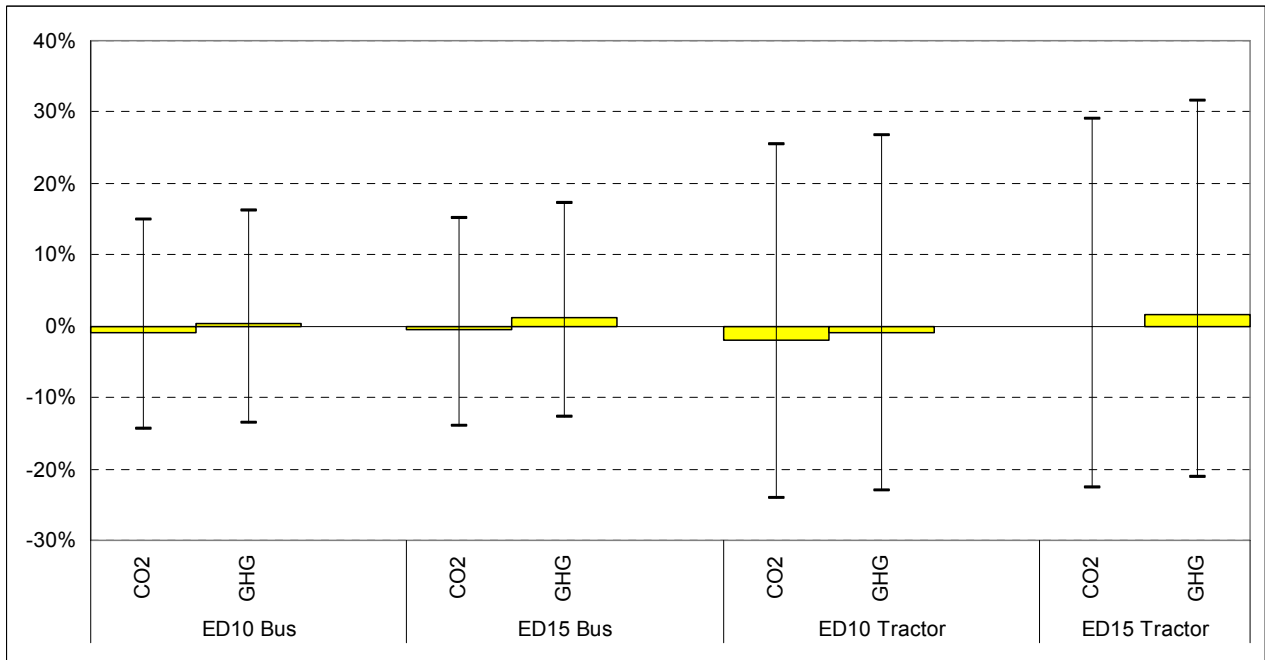


(b) Urban Buses (g/mi)

**Figure 5.** Well-to-Wheels PM<sub>10</sub> Emissions of Farming Tractors and Urban Buses

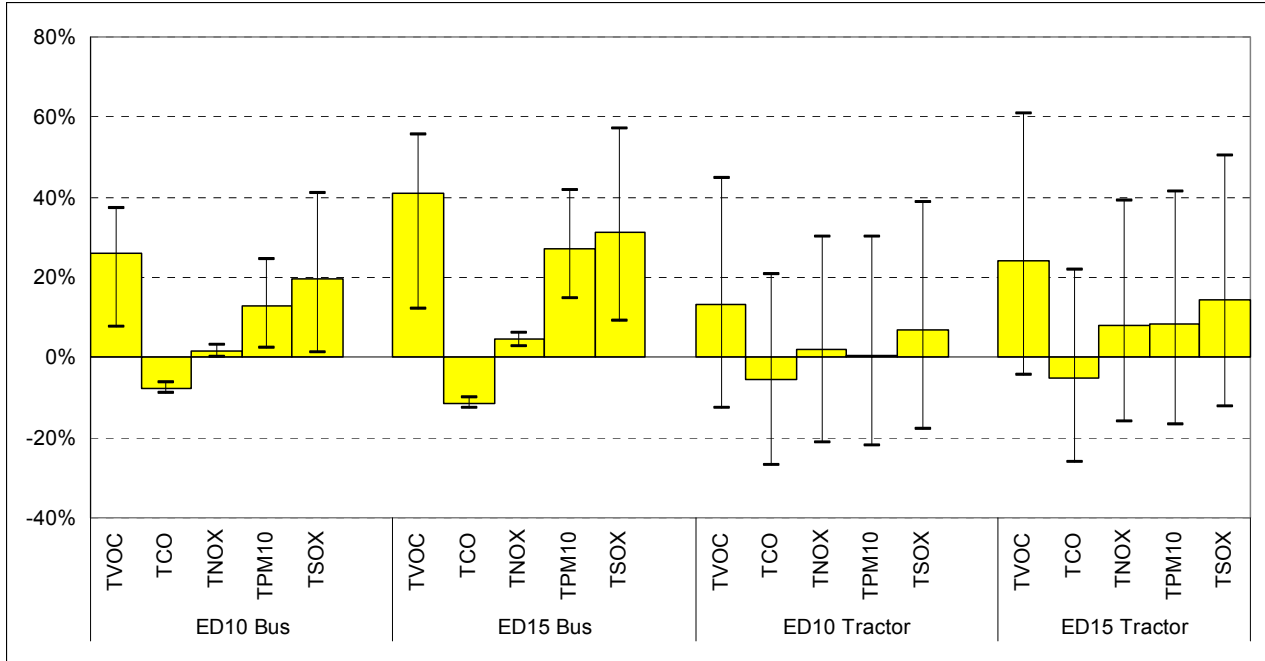


(a) Well-to-Wheels Energy Use Changes

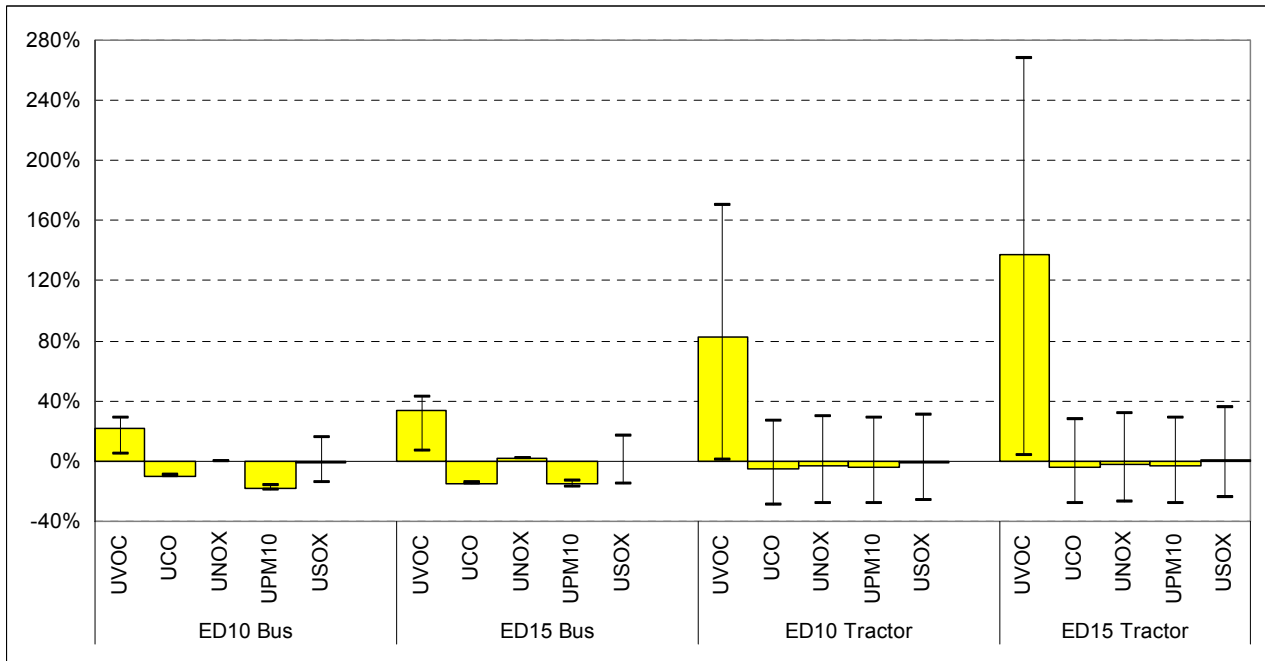


(b) Well-to-Wheels GHG Emission Changes

**Figure 6.** Well-to-Wheels Energy Use and GHG Emission Changes of Farming Tractors and Urban Buses (results are relative to those of tractors fueled by CD and buses fueled by LSD)



**Figure 7.** Well-to-Wheels Changes in Total Criteria Pollutant Emissions of Farming Tractors and Urban Buses (results are relative to those of tractors fueled by CD and buses fueled by LSD)



**Figure 8.** Well-to-Wheels Changes in Urban Criteria Pollutant Emissions of Farming Tractors and Urban Buses (results are relative to those of buses fueled by LSD)

## Conclusions

Using Argonne's GREET model, we conducted a WTW analysis of E-diesel blends vs. petroleum diesel for applications in farming tractors and urban buses. Our results show that use of ED10 or ED15 might result in increases in total energy use, but in reductions in fossil energy use and significant reductions in petroleum use relative to use of conventional or low-sulfur diesel fuel. In our total energy use calculations, energy consumption was taken into account for both ethanol and petroleum diesel, but in the calculations of fossil fuel and petroleum use, only energy in petroleum diesel was taken into account because the energy in ethanol is 100% renewable. The magnitude of the reduction in fossil fuel use by E-diesel blends is limited by the use of coal, natural gas, liquefied petroleum gas, diesel, and electricity during corn farming, ethanol production, and ethanol transportation.

Use of E-diesel blends relative to use of petroleum diesel results in few changes in GHG emissions — in contrast to GHG emission results showing moderate benefits for ethanol-gasoline blends vs. gasoline. This disparity is primarily caused by two factors. First, the WTP GHG emissions of diesel fuels are smaller than those of petroleum gasoline because WTP energy efficiencies for diesel fuels are higher than those for gasoline. Second, on an energy basis, while ethanol-gasoline blend use in ethanol-capable vehicles results in little fuel economy change relative to neat gasoline (despite ethanol-gasoline blends having somewhat lower *volumetric* fuel economy), E-diesel blends offer *heating value-based* fuel economy that is lower than that of petroleum diesel.

Our analysis shows that the most noteworthy benefits of E-diesel use lie with petroleum reductions and reductions in urban PM<sub>10</sub> and CO emissions by urban bus operations. We acknowledge that the overall effect of farming tractors and urban buses on the nation's petroleum use is tiny, and that urban CO emissions are increasingly becoming a non-issue for major U.S. cities. However, specifically with respect to pollution abatement, E-diesel could be a non-trivial asset of fuel portfolios for urban buses needing to reduce their PM<sub>10</sub> emissions.

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## **Appendix A: Energy Use and Emissions of Fertilizer Production**

Energy use and emissions data for fertilizer production were obtained from a report by the U.S. Department of Energy (DOE 2000), from publications by the European Fertilizer Manufacturers Association (EFMA 1995; 2000a, b, c, d), and from the annual survey by The Fertilizer Institute (TFI 2001). The DOE report provides relatively complete data on energy use and emission factors. Neither the DOE report nor subsequent communications with Energetics, the report contractor, could confirm whether lower or higher heating values were used. It appears that no uniform set of values was applied in the DOE report. In most cases, DOE did not present information on the amount of feedstocks used for fertilizer production. The EFMA publications provide a more detailed description of fertilizer production processes, but data on feedstock use, process energy consumption, and emissions are not complete. However, EFMA explicitly states that LHVs were used in its publications. The TFI survey provides fuel and electricity use for fertilizer production. Because NG is both a feedstock and a fuel in the production of ammonia fertilizer, DOE and TFI provided only aggregate (not allocated) NG use for ammonia production.

Production of ammonium nitrate and urea requires the use of ammonia as the major feedstock. It is therefore necessary to include process energy and emissions associated with ammonia production in estimating the energy use and emissions of these nitrogen fertilizers.

### **Data Sources**

Table A1 presents energy and emission data for ammonia production, Table A2 for urea production, Table A3 for nitric acid production, Table A4 for ammonium nitrate production, Table A5 for sulfuric acid production, Table A6 for phosphoric rock production, and Table A7 for phosphoric acid production. In these tables, blank cells mean that no data were available from a given study.

**Table A1.** Feedstock Use, Energy Use and Emissions for Ammonia Production (per ton of ammonia produced)

	<b>DOE (2000)</b>	<b>EFMA (2000a)</b>	<b>TFI (2001)</b>	<b>Krupp Uhde<sup>c</sup></b>	<b>Synetix<sup>c,d</sup></b>	<b>Kellogg, Brown&amp;Root<sup>c,d</sup></b>
<b>Feedstock (ton)</b>						
NG	0.46 <sup>a</sup>	0.463	0.46 <sup>a</sup>	0.46 <sup>a</sup>	0.46 <sup>a</sup>	0.46 <sup>a</sup>
<b>Process Energy (mmBtu)</b>						
NG and other fuels	3.556	6.193–7.739 <sup>b</sup>	11.371	5.034	4.494–6.294	6.094–7.094
Electricity	1.838		0.389			
Total process fuels	5.394	6.205–7.755	11.760	5.034	4.494–6.294	6.094–7.094
<b>Process-Related Emissions (lb)</b>						
CO	15.8	0.06				
CO <sub>2</sub>	2446.8	1000.0				
NO <sub>x</sub>		2.0				
TOC	9.44					
SO <sub>2</sub>	0.058	0.02				

<sup>a</sup> This value was obtained from mass balance estimates in Brown et al. (1996).

<sup>b</sup> This value is for ammonia produced by using conventional reforming technology. The EFMA did not separate total process fuel use into NG and electricity. We assumed all the process fuels estimated by the EFMA were NG.

<sup>c</sup> From *Hydrocarbon Processing* (1999).

<sup>d</sup> From *Hydrocarbon Processing* (2001).

Note that in Table A1, the averaged total NG (and other fuel) consumption value obtained by TFI is significantly higher than the value from other data sources. Assuming that the same amount of NG reported by the other sources was used as a feedstock for ammonia production, a much higher requirement for process fuel can be inferred in the TFI survey. This assumption will significantly affect emissions for the production of other nitrogen fertilizers, when emissions from combustion are accounted for. The TFI data were considered in our high-energy-use case (see Tables 4 and 5 in report).

**Table A2.** Feedstock Use, Energy Use, and Emissions of Urea Production (per ton of urea produced)

	DOE (2000)	EFMA (2000b)	Snamprogetti <sup>c</sup>
Feedstock (ton)			
Ammonia	0.567 <sup>a</sup>	0.57	0.566
Process Energy (mmBtu)			
NG and other fuels	1.464	2.816 <sup>b</sup>	2.679
Electricity	0.212	0.046	0.065
Total process fuels	1.676	2.862	2.744
Process-Related Emissions (lb)			
PM (uncontrolled)	241	45	
PM (controlled)	0.234	0.65	

<sup>a</sup> This value was based on stoichiometric calculations of mass balance.

<sup>b</sup> We estimated the process energy use on the basis of the steam consumption value provided in the EFMA (2000b) and steam temperature from the Snamprogetti process.

<sup>c</sup> From *Hydrocarbon Processing* (1999).

**Table A3.** Feedstock Use, Energy Use, and Emissions of Nitric Acid Production (per ton of nitric acid produced)

	DOE (2000)	EFMA (2000c)
Feedstock (ton)		
Ammonia	0.405 <sup>a</sup>	0.405 <sup>a</sup>
Process Energy (mmBtu)		
NG and other fuels	0.526	
Electricity	0.006	
Total process fuels	0.532	
Process-Related Emissions (lb)		
NO <sub>x</sub> (uncontrolled)	33.5	30.12
NO <sub>x</sub> (controlled)	2.2	1.21
N <sub>2</sub> O (uncontrolled)	11 <sup>b</sup>	3.63-51.48 <sup>c</sup>

<sup>a</sup> This value was based on stoichiometric calculations of mass balance.

<sup>b</sup> From IPCC (1996).

<sup>c</sup> Calculated on the basis of reported concentration of N<sub>2</sub>O in exhaust gases.

**Table A4.** Feedstock Use, Energy Use, and Emissions of Ammonium Nitrate Production (per ton of ammonium nitrate produced)

	<b>DOE (2000)</b>
Feedstock (ton)	
Ammonia	0.213 <sup>a</sup>
Nitric acid	0.788 <sup>a</sup>
Process Energy (mmBtu)	
NG and other fuels	0.440
Electricity	0.242
Total process fuels	0.682
Process-Related Emissions (lb)	
PM (uncontrolled)	528.065
PM (controlled)	4.662

<sup>a</sup> These values were based on stoichiometric calculations of mass balance.

**Table A5.** Feedstock Use, Energy Use, and Emissions of Sulfuric Acid Production (per ton of sulfuric acid produced)

	<b>DOE (2000)</b>	<b>TFI (2001)</b>
Feedstock (ton)		
Sulfur		0.325
Process Energy (mmBtu)		
NG and other fuels	0.060	0.029
Electricity	0.056	0.071
Total process fuels	0.116	0.100
Process-Related Emissions (lb)		
SO <sub>2</sub>	40 <sup>a</sup>	

<sup>a</sup> Based on emissions for the conversion efficiency of 97% from SO<sub>2</sub> to SO<sub>3</sub>.

**Table A6.** Energy Use of Phosphoric Rock Production (mmBtu/ton)

	<b>TFI (2001)</b>
NG and other fuels	
Electricity	0.245
Total process fuels	0.245

**Table A7.** Feedstock Use and Energy Use of Phosphoric Acid Production (per ton)

	<b>DOE (2000)</b>	<b>EFMA (1995)</b>	<b>TFI (2001)</b>
Feedstock (ton)			
Sulfuric acid			2.674
Phosphoric rock		2.6–3.5	3.525
Process Energy (mmBtu)			
NG and other fuels	2.972	1.546–6.800 <sup>a</sup>	
Electricity	0.650	0.371–0.557	0.481
Total process fuels	3.622	1.917–7.357	0.481

<sup>a</sup> Calculated on the basis of reported steam consumption. Steam was assumed to be at 1 bar and 200°C.

## **Appendix B: Nitrous Oxide Emissions from Nitrogen Fertilizer Applications in Corn Fields**

### **Current N<sub>2</sub>O Emission Values**

Assumptions in previous GREET versions concerning N<sub>2</sub>O flux from soils under corn cultivation are derived from a review of over 30 publications dating from 1997 and earlier (see Wang et al. 1997). The review concentrated on (1) direct N<sub>2</sub>O emissions from soil and (2) nitrogen bound as N<sub>2</sub>O and converted from leached nitrates in drainage and runoff water by means of microbial denitrification.

In general, the reviewed studies focused on the fate of the nitrogen in applied N-fertilizers over an entire growing season across several different growing regimes. Based on that review, We determined parametric assumptions for calculating N<sub>2</sub>O emissions in cornfields. Table B1 summarizes the resulting values adopted for the GREET model. For comparison, we also show IPCC's corresponding values in the table. Our and IPCC N<sub>2</sub>O emission values differ chiefly in the indirect emissions from nitrate leaching. Data from U.S. cornfields, as reviewed by us, showed a lower leaching rate and much lower conversion rate from nitrate to N<sub>2</sub>O. It should be noted that our review focused on U.S. Midwest cornfields, while the IPCC values could be intended to represent agricultural fields for all crops worldwide.

Both our 1997 review and the IPCC study conceded large uncertainties in N<sub>2</sub>O emissions. The sources of uncertainty include the following: (1) lack of uniform control measurement of background N<sub>2</sub>O, (2) failure of any single study to measure both direct-to-air N<sub>2</sub>O and N<sub>2</sub>O from leachate, (3) variable nitrate conversion rates and incomplete conversion for surface water and ground water, and (4) varying estimates of N<sub>2</sub>O solubility in water. Because of these underlying factors, uncertainties in N<sub>2</sub>O emissions will continue to exist.

**Table B1.** Soil N<sub>2</sub>O Emissions in Agricultural Fields

Item	N <sub>2</sub> O Emissions: Range Values (%)	N <sub>2</sub> O Emissions: Point Values (%)
Wang et al. 1997 (for U.S. midwest corn fields)		
Direct N <sub>2</sub> O air emissions: N <sub>2</sub> O-N as % of N in N-fertilizer	0–3.15	1.22
N loss in leached nitrate: nitrate-N as % of N in N-fertilizer	12–26.6	24
Nitrate to N <sub>2</sub> O conversion: N <sub>2</sub> O-N as % of leached nitrate-N	1	1
<b>Total</b>		1.46
IPCC 1996 (potentially for all crop lands worldwide)		
Direct N <sub>2</sub> O air emissions: N <sub>2</sub> O-N as % of N in N-fertilizer	0.25–2.25	1.25
N loss in leached nitrate: nitrate-N as % of N in N-fertilizer	30	30
Nitrate to N <sub>2</sub> O conversion: N <sub>2</sub> O-N as % of leached nitrate-N	0.2–12	2.5
Gasification of N-fertilizer to NO <sub>x</sub> and NH <sub>3</sub>	10	10
N <sub>2</sub> O-N from gasified NO <sub>x</sub> and NH <sub>3</sub>	0.2–2	1
<b>Total</b>		2.1

### Additional Issues Regarding N<sub>2</sub>O Emissions

The studies reviewed for our 1997 analysis did not explicitly address N<sub>2</sub>O flux behavior outside of the growing season. Recent investigations of off-season N<sub>2</sub>O flux have indicated that significant N<sub>2</sub>O emissions can occur during freeze/thaw cycles in winter and early spring (pre-planting). Kaiser and Heinemeyer (1996) reported the results of a two-year study of sandy and silty loam crop soils in Germany that identified peak rates of N<sub>2</sub>O emission at (1) spring thaw and (2) within one week after N-fertilizer application. Emission intensity was approximately equal during both types of episodes. Flessa and Dorsch (1995) reported that the highest N<sub>2</sub>O release rates measured during their experiments with wheat-growing soils in southern Germany occurred during January-February thaws. However, Flessa and Dorsch pointed out that “high N<sub>2</sub>O fluxes may occur from cultivated soils even if no mineral N-fertilizer is applied.” This could imply that significant N<sub>2</sub>O releases are caused by factors, other than N-fertilizer applications, that occur during freeze/thaw cycles.

Table B1 shows a large discrepancy in estimates of indirect N as N<sub>2</sub>O emissions due to denitrification. While GREET shows an N<sub>2</sub>O emission rate of 0.24%, IPCC shows a rate of 0.75%. A recent detailed study on nitrate-to-N<sub>2</sub>O emissions in the United Kingdom (Silgram et al., 2001) indicated that the IPCC might have overestimated the indirect N<sub>2</sub>O emissions by a large margin. With detailed soil simulations in the United Kingdom, the authors concluded that IPCC’s estimates are 2.25 times higher than U.K. estimates, even though the authors used the IPCC conversion factor of 2.5% from nitrate to N<sub>2</sub>O. If the IPCC conversion rate is adjusted with the U.K. results, the indirect N<sub>2</sub>O emission rate would be 0.33% ( $0.75\% \div 2.25$ ).

Another source of N<sub>2</sub>O emissions from agricultural fields, one that we did not include, is crop residues. IPCC (1996) maintained that 0.015 kg of N is produced in the soil per kg of dry biomass left in the field. We use corn as an example to demonstrate the magnitude of nitrogen from crop residues. Assuming the yield ratio of corn kernels to corn stover to be 1 to 1 on a dry-



mass basis, harvesting a bushel of corn could result in production of 21 kg (the dry weight of a bushel of corn) of dry corn stover. This will result in 0.315 kg of nitrogen in the soil per bushel of corn harvested ( $0.015 \times 21$ ). On the other hand, the N-fertilizer application rate for U.S. corn farming is about 0.47 kg N-fertilizer per bushel of corn (see Table 6). Thus, the amount of nitrogen to soil from corn residues is about 2/3 of that from N-fertilizer applications. However, emissions from the nitrogen in biomass should already be taken into account with measured N<sub>2</sub>O emissions from cornfields when crop residues are not removed from fields, as is the case for most U.S. corn farms.

### **Parametric Assumptions for GREET Simulations**

Considering the potential N-fertilizer-induced N<sub>2</sub>O emissions outside of growing seasons and a small increase in indirect N<sub>2</sub>O emissions from nitrate, we have increased N<sub>2</sub>O emissions for our new “point estimate” from 1.5% to 2.0%, with a range of 1% to 3%.