Comparison of Achievable Magnetic Fields with Superconducting and Cryogenic Permanent Magnet Undulators – A Comprehensive Study of Computed and Measured Values*

Light Source Note: ANL/APS/LS-348 E.R. Moog, R.J. Dejus, and S. Sasaki

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^{*} Work supported by the U.S. Department of Energy, Office of Science, under Contract No. DE-AC02-06CH11357.

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Revisions: Original release July 17, 2017.

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Abstract

Magnetic modeling was performed to estimate achievable magnetic field strengths of superconducting undulators (SCUs) and to compare them with those of cryogenically cooled permanent magnet undulators (CPMUs). Starting with vacuum (beam stay-clear) gaps of 4.0 and 6.0 mm, realistic allowances for beam chambers (in the SCU case) and beam liners (in the CPMU case) were added. (A 6.0-mm vacuum gap is planned for the upgraded APS). The CPMU magnetic models consider both CPMUs that use NdFeB magnets at ~150 K and PrFeB magnets at 77 K. Parameters of the magnetic models are presented along with fitted coefficients of a Halbach-type expression for the field dependence on the gap-to-period ratio. Field strengths for SCUs are estimated using a scaling law for planar SCUs; an equation for that is given. The SCUs provide higher magnetic fields than the highest-field CPMUs – those using PrFeB at 77 K – for period lengths longer than ~14 mm for NbTi-based SCUs and ~10 mm for Nb₃Sn-based SCUs. To show that the model calculations and scaling law results are realistic, they are compared to CPMUs that have been built and NbTi-based SCUs that have been built. Brightness tuning curves of CPMUs (PrFeB) and SCUs (NbTi) for the upgraded APS lattice are also provided for realistic period lengths.

Introduction

Cryogenic permanent magnet undulators (CPMUs) are the extension to lower temperatures of the well-established in-vacuum undulators. At cryogenic temperatures, permanent magnets produce higher magnetic field and are more radiation-resistant than at room temperature, advantages that make CPMUs appealing and, as a result, increasingly common worldwide [1,2,3]. Comparisons of future undulator technologies for use in storage rings and free electron lasers have been extensively reported in the literature – for good overviews see papers by Bahrdt [4], Couprie [5], and Chavanne [6].

At the Advanced Photon Source (APS), superconducting technology was chosen as a means of achieving enhanced undulator capabilities. The first superconducting undulator (SCU), called SCU0, to be installed in the APS storage ring was successfully commissioned in January 2013 [7]. As technology development proceeded, the SCU0 was followed by the SCU18#1 and the SCU18#2, both 18-mm-period undulators with a magnetic length of 1.1 m, in 2015 and 2016, respectively [8]. The SCU0 was replaced by the longer SCU18#2 after 3.5 years of continuous successful operation in the storage ring.

The various undulator technologies have different advantages, but one of the most important aspects of an undulator is the strength of the magnetic field as a function of undulator gap and period length. Insertion devices (IDs) with short period lengths offer increased brightness and flux, but come with the trade-off of a reduced magnetic field strength. A high magnetic field strength provides extended harmonic energy tuning ranges. Here we focus on the comparison of computed magnetic field strengths achievable over a range of period lengths with both technologies under realistic conditions and on comparing those strengths with measured values. This study covers primarily SCUs fabricated with NbTi superconducting wires since all

undulators installed in storage rings to date use this material. It is important to note, however, that successful construction and stable operation of Nb₃Sn-based SCUs in storage rings will offer the possibility of much higher magnetic fields for the same period length. (Work has begun in this direction but no experimental results or fabrication challenges are reported on in this study.)

The interest in cryogenic permanent magnet materials comes from the increase in remanent field and coercivity of the permanent magnets at low temperatures, providing both higher magnetic field and higher resistance to radiation-induced demagnetization of the magnet compared to room-temperature operation. The newer grades of PrFeB show higher performance than the grades of NdFeB because, unlike NdFeB, there is no spin reorientation transition at ~150 K, so operation at colder temperatures becomes advantageous. (The spin reorientation reduces the on-axis undulator field if magnets are cooled below the transition temperature.) As a result, many recent undulators are constructed with PrFeB magnets [9]. This study presents results for both magnet materials. Further, a comprehensive literature review was undertaken with key results summarized in tables for quick access at the end.

Magnetic Computer Models

Calculations were carried out using the OPERA-3D code [10] to estimate the field strength achievable with a cryogenic permanent magnet undulator. Models using both PrFeB and NdFeB magnets were explored for a hybrid configuration, with vanadium permendur poles between the magnets. Choices made in the design were aimed at making the field of the CPMU large without being inconsistent with the range of fabricated undulators. One example of such a choice is selecting strong magnet grades.

The magnetic parameters used for PrFeB were those of grade NMX-68CU from the Neomax Engineering subsidiary of Hitachi Metals, which is being used at the Taiwan Photon Source (TPS) [11]. For NdFeB, the magnetic parameters used were those of grade NMX-S45SH, also from Neomax. This is the grade chosen for the CPMU at the Swiss Light Source (SLS) [12]. Both of these grades are either the strongest or very close to the strongest grades used in existing CPMUs. The important magnetic characteristics are summarized in Table 1.

Table 1. Magnetic characteristics of the NdFeB and PrFeB magnet grades used in the computer models. Note that cryogenic NdFeB operation was set at a temperature of \sim 150 K to avoid the reduction in B_r due to spin reorientation at lower temperatures.

Material	Temp	B _r (T)	H _{cB} (kA/m)	H _{cB} (Oe)	H _c (kA/m)	H _c , (Oe)
PrFeB NMX-68CU	77 K	1.67	1240	15582	6200	77911
PrFeB NMX-68CU	295 K	1.40	1010	12692	1680	21112
NdFeB NMX-S45SH	150 K	1.50	1137	14288	4000	50265
NdFeB NMX-S45SH	293 K	1.30	970	12200	1671	21000

The vanadium permendur B-H curve used for the pole material was the same as that used for the room-temperature undulator field calculations at APS. It gives good agreement with the finished APS devices. No changes have been made to adapt it for cryogenic temperatures, but it is expected to be a good approximation. Data on temperature dependence received from Vacuumschmelze shows a very small difference (less than 1%) in μ_r between 80 °C and -30 °C (minimum listed temperature) for H above about 3 Oe. (A temperature of 150 K is about as far from room temperature as -30 °C is from 80 °C, so to the extent that the magnetic response can be extrapolated to ~150 K, the established numbers for μ_r at room temperature are expected to be reasonably good.)

Results

Computed Magnetic Fields of Cryogenic Permanent Magnet Undulators (CPMUs)

The magnetic designs are intended to be realistic with the emphasis on building an undulator with a strong magnetic field. Other considerations, such as not demagnetizing the magnets during assembly or bakeout (in case a bakeout procedure is required), or minimizing the overall height of the parts of the undulator that need to fit into a vacuum chamber, may lead to other design choices. Dimensions used for the magnets and poles, such as the pole and magnet widths and the magnet overhang on the back of the poles, are similar to those used for conventional short-period undulators at the APS. Further optimization of most of the dimensions would not have a strong impact on the on-axis effective or peak magnetic fields. Those dimensions that would have a larger impact on achieving the highest undulator field, i.e., the thicknesses (in the beam direction) of the magnet and pole, have been optimized for each design. The overall dimensions of magnets and poles and results of design optimizations are summarized in Table 2 for 4 different period lengths (0.8, 1.1, 1.5, and 2.0 cm).

Table 2. Summary of parameters for models and results for two magnetic gaps: 0.42 cm and 0.62 cm. Optimizations were performed at 0.42 cm gap. H_{zworst} is the worst demagnetizing field seen by the magnet. The coordinate system is defined such that x is in the transverse horizontal direction, y is in the vertical direction, and z is the longitudinal (beam) direction.

		ALL DIN	IENSIONS I	N CM						
	dimensions for all				Beff (G) at	Bpeak (G) at	Hzworst (Oe)	Beff (G) at	Bpeak (G) at	Hzworst (Oe)
material	models	period	magnet z	pole z	0.42 cm gap	0.42cm gap	0.42 cm gap	0.62 cm gap	0.62cm gap	0.62 cm gap
PrFeB NMX-68CU 77K		0.8	0.251	0.149	5823.7	5856.2	16582.6	2624.8	2631.9	16671.3
Br= 16700 G	magnet x = 6.4	1.1	0.333	0.217	9347.9	9424.6	17725.9	5122.9	5138.4	17906.1
Hcb = 15582 Oe	magnet y = 5.0	1.5	0.461	0.289	13071.2	13310.0	17805.0	8435.1	8499.1	18909.3
Hcj = 77911 Oe	pole x = 4.4	2	0.535	0.465	16723.8	16520.8	18748.9	11448.2	11327.1	19934.9
	pole y = 4.2									
NdFeB NMX-S45SH 150 K	all chamfers = 0.02	0.8	0.262	0.138	5465.3	5505.5	15316.2	2459.3	2467.0	15355.6
Br= 15000 G	no magnet recess	1.1	0.344	0.206	8809.0	8913.8	16622.6	4784.9	4805.6	16572.6
Hcb = 14288 Oe		1.5	0.438	0.312	12463.0	12561.2	17734.0	7643.8	7662.5	17643.2
Hcj = 50265 Oe		2	0.546	0.454	15877.0	15771.9	18030.0	10642.4	10560.2	18613.5

As can be seen in the table, the optimal magnet thickness varies with the choice of magnet material and period. For each case the optimization was performed at the minimum gap of 0.42 cm. The column labeled 'H_{zworst}' is the worst demagnetizing field in the magnet at a gap of 0.42 cm or 0.62 cm. (The demagnetizing field may be worse than this at another gap larger than 0.42 cm.)

A difference from the standard APS undulator designs is that the magnet tip is not recessed relative to the pole tip. (APS undulators typically have the pole tip extending 0.05 cm further towards the beam than the magnet tip; this provides space for placement of shims on the magnet tips without affecting the minimum gap. It reduces the on-axis field of the undulator, however.) Another difference from the standard APS undulator designs is that chamfers at the edges of the magnets and poles have been reduced to 0.02 cm, i.e., just small enough to remove any sharp edges. In a more complete design intended for construction, some chamfering may be desired to help reduce the highest demagnetizing field in the magnets. For example, such a choice was made by Bahrdt et al. [13].

Note that space constraints inside a vacuum chamber, or other considerations, may restrict the height of the magnets and poles to smaller values than those used here, with some cost in magnetic field strength. The present choice of the magnet height of 5 cm is where the increase in field strength with height flattens, as shown in Fig. 1. As will be discussed in the section "Comparison of Generic CPMU Model Calculations to Real Undulators" the magnet heights chosen for the CPMUs that have been built (and for which magnet dimensions were published) are indeed shorter. The pole is assumed to be 0.8 cm shorter than the magnet; this is close to the values found in thoroughly optimized APS models with taller magnets, and it is also the value chosen for the CPMU at SOLEIL [9]. The difference in B_{eff} between a magnet height of 3 cm and 5 cm is about 1% (see Fig. 1).



Fig. 1. Calculated effective magnetic field of the 1.5-cm-period undulator at the minimum gap of 0.42 cm for different values of the magnet height for the PrFeB magnet model. The pole is assumed to be 0.8 cm shorter than the magnet. A magnet height of 5.0 cm was chosen for the model computations.

An example of the optimization of the thickness of the magnet is shown in Fig. 2. The choice of magnet thickness also determines the pole thickness since the combined thickness is half of the period length.



Fig. 2. An example of the optimization of the magnet thickness (in the beam direction). The effective magnetic field for the 0.8-cm-period PrFeB model is shown at the minimum gap of 0.42 cm. The orange line marks the chosen magnet thickness of 0.251 cm.

The optimized results for the peak and effective fields were further cross-checked using the code RADIA [14]. The Nd results agreed within $\sim 2\%$. The Pr results varied a little more, but still agreed to better than 5%.

Comparison of Magnetic Fields of CPMUs, Superconducting Undulators (SCUs), and an In-Vacuum SmCo Undulator (IVU)

The computed on-axis effective and peak magnetic fields of the modeled CPMUs (PrFeB and NdFeB) optimized at 0.42 cm gap (see Table 2) were fitted to an equation of the form

$$B_{fit} = a * \exp\left(-br + cr^2\right),\tag{1}$$

with unknown coefficients a, b, and c, where r = magnetic gap/period. The fit is shown in Fig. 3, and the derived coefficients for the different cases are given in Table 3.



Fig. 3. Comparison of computer-modeled values of the effective magnetic fields for CPMUs based on NdFeB and PrFeB magnets, with fitted curves (B_{eff} is from Table 2 for a magnetic gap of 4.2 mm; coefficients used for B_{eff} are from Table 3).

Table 3. Fitted coefficients of the effective and peak magnetic fields from model calculations to an expression of the form $B_{fit} = a * \exp(-br + cr^2)$. The two numbers given are for the effective field (B_{eff,fit}) and peak field (B_{peak,fit}), respectively.

Magnet grade	Material	Temp.	$a_{Beff} / a_{B_{peak}}$	$b_{Beff}^{}/b_{B_{peak}}^{}$	$c_{Beff}^{}/c_{B_{peak}}^{}$
NMX-68CU	Pr ₂ Fe ₁₄ B	77 K	3.502 / 3.198	-3.604 / -3.062	0.359 / -0.332
NMX-S45SH	Nd ₂ Fe ₁₄ B	150 K	3.341 /3.121	-3.606 / -3.204	0.300 / -0.193

A similar parameterized fit was done previously for an in-vacuum SmCo undulator (IVU) assuming the use of Shin-Etsu's magnet grade R32HS, yielding the fit

$$B_{eff,fit} = 2.940 * \exp\left(-4.62r + 1.37r^2\right), \qquad (2)$$

where *r* is the ratio of magnetic gap/period [15].

For planar SCUs the scaling law [16] was used to calculate the magnetic fields of different period lengths λ_u and magnetic gaps (g). For NbTi superconducting wires the parameterization at 80% of the critical current density J_c is:

$$B_o = \left[0.28052 + 0.05798\lambda_u(mm) - 0.0009\lambda_u^2(mm) + 5 * 10^{-6}\lambda_u^3(mm)\right] * \exp\left[-\pi \left(\frac{g(mm)}{\lambda_u(mm)} - 0.5\right)\right]$$
(3)

where g is the magnetic gap of the SCU and λ_u is its period.

For Nb₃Sn superconducting wires the same expression was used but with the magnetic field enhanced by a multiplicative factor of 1.3. No distinction was made between the effective and peak magnetic fields but for all practical purposes they are considered the same because any differences are very small (<1%).

Eq. 1 and the coefficients of Table 3 were used to compute, versus period length, the magnetic fields of CPMUs based on the two different magnet materials for two different vacuum gaps (beam stay-clear gaps): 4.0 mm and 6.0 mm (using magnetic gaps described below). The smallest vacuum gap of 4.0 mm represents a typical small-gap operation of a CPMU installed on a third-generation storage ring. The 6.0-mm vacuum gap represents a gap feasible for the upgraded APS (APS-U).

The magnetic gap must be slightly larger than the vacuum gap. For the CPMUs there is a thin beam liner installed on top of the magnets and poles so that the beam sees a smooth surface for low impact on the beam impedance. The liner is typically made of a Ni-plated Cu foil with a thickness of 100 μ m. A gap increase of 200 μ m allows for the top and bottom liners. For the SCUs, a thin-wall vacuum chamber with a wall thickness of 0.6 mm and an insulating gap of 0.3 mm adds up to a total gap allowance of 1.8 mm, taking a vacuum gap of 6.0 mm to a magnetic gap of 7.8 mm. While this allowance is 0.5 mm smaller than for the existing SCUs installed in the APS storage ring (where the vacuum gap is 7.2 mm, the vacuum chamber wall thickness is 0.65 mm top and bottom, and the insulating gap is 0.5 mm top and bottom, making for a magnetic gap of 9.5 mm), it uses the new 0.6-mm thickness of the ID vacuum chambers being prototyped for the APS-U out-of-vacuum undulators. This 0.6-mm thickness will also be adopted for future SCUs at APS. At ANKA, a beam liner is used that allows for only a 1-mm difference between the vacuum and magnetic gaps [17].

As to the feasibility of installing IVUs in the APS-U storage ring with the new multi-bend achromat lattice, estimates for a vacuum gap of ~ 6.0 mm show that there is not a significant impedance impact from an IVU. The relative impedance contributions from the ID transitions are markedly reduced in the new lattice as compared to the existing APS lattice. However, a lot of the particulars depend on the actual IVU transition designs, and to what extent the conducting foils placed on the magnets work as intended [18].

The calculated fields of the CPMUs are compared to the previously computed magnetic fields of a SmCo IVU and the NbTi and Nb₃Sn SCUs in Figs. 4 (a) – (c) for a vacuum gap of 4.0 mm and in Figs. 5 (a) – (c) for a vacuum gap of 6.0 mm.

As can be seen, the SCUs give the highest on-axis magnetic fields for period lengths longer than a certain threshold value. The exact value depends on details in the underlying assumptions. Here it occurs at ~14 mm for NbTi and ~10 mm for Nb₃Sn (and essentially independent of the magnetic gaps chosen here). The threshold period length is probably smaller in reality because the SCUs here are assumed to operate at 80% of the critical current density but could in principle be operated at higher currents. Also, the parameters of the computed CPMU models were selected to give generous estimates of the CPMU fields. As discussed below, those estimates, when compared to CPMUs that have been built, are overestimates.



Fig. 4a. Calculated on-axis magnetic fields of two CPMUs (PrFeB, NdFeB), two SCUs (NbTi, Nb₃Sn), and one IVU (SmCo) for a *vacuum gap of 4.0 mm* for period lengths from 8 mm to 30 mm.



Fig. 4b. Close up view of the short-period region from Fig. 4a.



Fig. 4c. Ratio of the magnetic field of SCUs to that of PrFeB-based CPMUs; from data in Fig. 4a.



Fig. 5a. Calculated on-axis magnetic fields of two CPMUs (PrFeB, NdFeB), two SCUs (NbTi, Nb₃Sn), and one IVU (SmCo) for a *vacuum gap of 6.0 mm* for period lengths from 8 mm to 30 mm. A 6-mm vacuum gap is feasible for the APS-U.



Fig. 5b. Close up view of the short-period region from Fig. 5a.



Fig. 5c. Ratio of the magnetic field of SCUs to that of PrFeB-based CPMUs; from data in Fig. 5a.

First Harmonic Energies and Brightness Tuning Curves for Undulators Installed on APS-U

A higher magnetic field for a given period length means that the energies of the harmonics will be lower. This is illustrated in Fig. 6, which shows the calculated first harmonic energies at 6 GeV beam energy for a NbTi-based SCU and a PrFeB-based CPMU for period lengths 14 - 20 mm, which are important for the APS-U. A vacuum gap of 6.0 mm was assumed, which is realistic for the APS-U (the magnetic gaps are larger by the amounts discussed in the previous section). For example, a first harmonic energy of 11 keV can be reached for period lengths of 15.5 mm and 16.0 mm for the SCUs (NbTi) and the CPMUs (PrFeB), respectively.



Fig. 6. Calculated first harmonic energies for SCUs (NbTi) and CPMUs (PrFeB) for a vacuum gap of 6.0 mm at 6 GeV beam energy. The SCUs are assumed to be operating at 80% of the critical current density.

The calculated brightness tuning curves of SCUs (NbTi) and CPMUs (PrFeB) with suitable period lengths for the APS-U are shown in Fig. 7. A CPMU with a period length of 2.0 cm is required for continuous energy coverage between the first and third harmonics (frequently a desired feature for the APS users). However, if an SCU with a 1.85-cm period were chosen instead, both the lowest reachable first harmonic energy and the continuous energy coverage would be preserved with the added benefits of higher brightness and lower power. (An SCU with a 2.0-cm period length would reach a lower first harmonic energy along with higher emitted power.)

In a similar way, a CPMU with a period length of 1.6 cm can be compared with either a 1.6cm-period SCU or a 1.55-cm-period SCU. The 1.55-cm-period SCU would reach the same minimum first harmonic energy as the 1.6-cm-period CPMU, and have the same energy coverage range, but the brightness would be higher. Alternatively, the 1.6-cm-period SCU would provide the same brightness but the energy tunability range would extend to lower energy. This increased tunability range is especially pronounced in the higher harmonics.



Fig. 7. Calculated brightness tuning curves of odd harmonics for CPMUs (PrFeB – solid curves) and SCUs (NbTi – dotted curves) for the APS-U 42-pm lattice for 6 GeV beam energy and 200 mA beam current. Magnetic lengths of 1.8 m were assumed with no limitations due to high heat loads imposed. The SCU is assumed to be operating at 80% of the critical current density. The period lengths were chosen to show the tradeoff between a shorter period device that keeps the same tuning range and gives higher brightness vs. keeping the same period length so the brightness stays the same but the energy tuning range is wider, especially for the higher harmonics. Considerations of lowest energy required and whether gaps in the tuning range are acceptable help guide the choices. Estimated reductions of higher harmonics due to magnetic field errors were applied.

Generic CPMU Model Calculations Compared to Real CPMUs

As stated above, the design decisions for the generic CPMU models were aimed at maximizing the magnetic field without straying very far from reality. To check the validity of the results, a comprehensive review of many of the existing and planned CPMUs worldwide was done. A summary of this is given in Tables 4 and 5 below, which show lists of real CPMUs, based on Nd or Pr magnets, respectively. Undulators that have been assembled and measured are included along with undulators in various stages of construction; the table states whether the values for the on-axis magnetic field are measured or computed for a particular magnetic design. There are separate columns for B_{eff} and B_{peak} , but the difference is small as can be seen for the few CPMUs where values of both were reported in the literature. (The generic model calculation results shown in Table 2 above also showed only a small difference.)

The tables also include calculated values of B_{eff} computed from Eq. 1 using the coefficients listed in Table 3, and the ratio of those values to the measured values or the design values if measurements are not yet available. As can be seen, the computed magnet field is larger than the measured magnetic field in every case except for two undulators that are still in development (so that measurements are not yet available), though the overestimate is in many cases by only a few percent. Cases with larger discrepancies can be because the real undulator's magnetic design was not intended to produce an optimized field; instead the undulator was primarily developed to check some technical aspect of the CPMU design. Also, some undulators were constructed with weaker magnets than those assumed in the generic calculations – especially those where the magnets needed to survive a bakeout procedure. Overall the generic CPMU models give reasonable estimates of the field that an ideal CPMUs can provide. They do not, however, allow for schemes to enhance the field using additional magnets on the sides or backs of the poles [46] or for alternative pole materials such as Dy [47].

SCU Scaling Law Compared to Real SCUs

The scaling law expression given in Eq. 3 of the magnetic field of planar SCUs can also be compared to existing SCUs. Table 6 shows the characteristics of SCUs at the ANKA synchrotron radiation source in Karlsruhe, Germany and the APS, and of the LCLS R&D SCU built at APS.

The scaling law assumes that the SCU is operating at 80% of the critical current. At the APS, the SCUs are operated close to 80% of the critical current (and sometimes higher) [7, 77], and the operating fields are within ~1% of the scaling law predictions. Thus, the magnetic field calculated from the scaling law has been experimentally demonstrated at the APS for all 4 undulators built to date. The operating point given for the ANKA SCU15 device [71] is ~60%, so its operating field is correspondingly lower than the scaling law prediction.

Conclusions

On-axis magnetic fields of planar CPMUs made of NdFeB and PrFeB permanent magnets and of SCUs made of NbTi and Nb₃Sn superconducting wires were computed. The computations were based on magnetic design calculations of generic CPMU models and on the scaling law for the SCUs. The computed fields were compared to undulators that have been built to verify that the computed field strengths are realistic. For the CPMUs it was found that the computed magnet fields were larger than the measured fields in nearly every case. For the NbTibased SCUs that are operated at 80% of the critical current (as the APS undulators are), the measured magnetic fields were within ~1% of predictions; the predictions assumed operation at 80%.

From this we can conclude with high certainty that NbTi-based SCUs with period lengths longer than ~14 mm and (although with less certainty) that Nb₃Sn-based SCUs with periods longer than ~10 mm provide the highest magnetic fields for realistic magnetic gaps installed in storage rings. The higher magnetic fields give the choice of extending the brightness tuning ranges of harmonic energies (for the same period length) or shortening the period length to increase the photon brightness (for the same tuning ranges). The period lengths planned for APS-U are 16 mm or longer thus making the SCU the preferred choice. SCUs also offer the possibility of future significant improvements in undulator field strength once the promise of Nb₃Sn conductors is realized.

Table 4. List of CPMUs based on NdFeB magnets. In the column labeled 'Ratio Calc/Meas', the measured value is used when available, otherwise the design value is used.

NdFeB	Magnet Grade & Supplier	Temp (K)	Br (T)	Hcj (kOe)	Magn. Gap (mm)	Period (mm)	No. of Periods	Overall Length (m)	B _{peak} (T)	B _{eff} (T)	Design or Measured	Magn. Dims: w x h x t (mm)	Pole Dims: w x h x t (mm)	Status	Gap / Period	B _{eff} Fit (T)	Ratio Calc/Meas	Reference(s)
Diamond Light Source (DLS)	Vacodym 776 TP	293 K	1.31	21	4	17.7	113	2.05		1.18	meas.		33 wide	installed	0.226			[19, 20]
(Built by Danfysik)	VAC	157 K			4					1.263	meas.			June 2010	0.226	1.502	1.19	
		293 K			10					0.37	meas.				0.565			
		157 K			10					0.402	meas.				0.565	0.479	1.19	
European Synchrotron Rad. Facility (ESRF)	Neorem 595t	150 K			6	18		2	0.892		design	50x30x6.2	32x24x2.8		0.333	1.038	1.16	[21 - 25]
1st CPMU; installed in ID6 test beamline	Neorem / VAC	150 K	1.28	54					0.881		meas.			installed	0.333	1.038	1.18	
Note: Poles are of low-carbon steel		300 K	1.17	27.6					0.821		meas.			Jan 2008				
European Synchrotron Radiation Facility	Vacodym 764	150 K	1.5		6	18		2	0.99		meas.			installed	0.333	1.038	1.05	[26, 27]
											meas.							
2nd CPMU; installed on ID11	VAC	293 K	1.33	16					0.907		@297K			2012				
National Synchrotron Light Source (NSLS)	Neomax 42AH	150 K	1.45		5.6	18	55	1.02	1.05		design			installed	0.311	1.120	1.07	[28, 29]
Cryo-ready MGU-X25	Neomax / Hitachi	293 K	1.28	24					0.9		meas.			Jan 2006				
NSLS 10-pole prototype		207 K			4.75	13.5	3.5	0.15	0.95		meas.				0.352	0.975	1.03	[28]
NSLS PPM prototype		201.6 K			6	16	18.5		0.623		meas.				0.375	0.901	1.45	[28]
Shanghai Synchrotron Rad. Facility (SSRF)	N48H	138 K	1.53	50	6	20	80		1.06	1.03	meas.	65x25x6.2	43x20x3.7	Feb 2015	0.300	1.164	1.13	[30]
Note: this N48H has (Nd:Pr = 3:1)	Zhejiang Innuovo	300 K	1.35	19.4					0.965	0.94	meas.							
SOLEIL 4-period test. First test.	Neomax 50BH	293 K	1.41	13.9	10	20	4		0.5		meas.	50x30x7.5	33x22x2.5		0.500			[31 - 35]
	Neomax/Hitachi	140 K		40					0.567		meas.				0.500	0.593	1.05	
		100 K		48					0.548		meas.				0.500			
SPring-8 CPMU prototype	Neomax 50BH	130 K	1.57		5	15	40	0.6	0.92		meas.				0.333	1.038	1.13	[2], [36 - 38]
Pure permanent magnet design	Neomax / Hitachi	300 K	1.43						0.805		meas.							
Spring-8 CPMU 15	NMX49CH	300 K	1.36	16		15		1.4						installed				[39, 40]
		150 K	1.48	38										Feb 2013				
Swiss Light Source (SLS) CPMU14	Neomax S45SH	135 K	1.5	50.3	4	14	120	1.7	1.15		meas.			2010	0.286	1.222	1.06	[12], [41 -
collab. between SPring-8, Hitachi, PSI	Neomax / Hitachi	135 K			3.5	14			1.3		meas.				0.250	1.382	1.06	43]
		293 K	1.3	≥21														

					Magn.			Overall				Magnet	Pole Dims.:					
	Magnet Grade &	Temp.		Hcj	Gap	Period	No. of	Length	B _{peak}		Design or	Dims: w x h	wxhxt		Gap /	$B_{\text{eff}}\ \text{Fit}$	Ratio	
PrFeB and (Pr, Nd)FeB	Supplier	(K)	Br (T)	(kOe)	(mm)	(mm)	Periods	(m)	(T)	B_{eff} (T)	Measured	x t (mm)	(mm)	Status	Period	(T)	Calc/Meas	Reference(s)
Diamond Light Source (DLS)																		
Planned: two new CPMUs	(Pr,Nd)FeB	80 K				17.6			1.2					in dev.				[20]
European Synchrotron Radiation Facility (ESRF)	Vacodym 131 DTP	80 K	≥1.58	>40	5	14.4		2	1		meas.	38x23x4.7	25x18x2.5	installed	0.347	1.046	1.05	[44 - 45]
3rd CPMU, installed on ID31.	PrFeB + GBD, VAC	293 K	≥1.38	>20.6										Jul 2016				
Helmholtz-Zentrum Berlin (HZB) collab. with	(Pr.8 ,Nd.2)2 Fe14 B	300 K			2.5	9	20		1.03	1.01	design	16x14x2.8	12x12x1.6	~2011	0.278			[13], [46 - 49]
Ludwig-Maximilian University München	VAC	30 K			2.5	9			1.15	1.12	design				0.278	1.323	1.18	
Fixed-gap prototype for Max-Planck-		300 K	1.42		2.5				0.996		meas.							
Institut für Quantenoptik, Garching		25 K	1.69		2.5				1.149		meas.				0.278	1.323	1.15	
Used at Mainzer Microtron, MAMI		300 K			2	9				1.28	meas.				0.222			
		30 K			2	9				1.43	meas.				0.222	1.600	1.12	
Helmholtz-Zentrum Berlin (HZB)	(Pr,Nd) ₂ Fe ₁₄ B with	293 K	1.38	20.6	2.5	9	11		1		meas.		14x14x2.44		0.278			[49, 50]
Prototype with side magnets integrated	GBD. VAC	77 K	1.62	67.1									in total					
into the poles		20 K							1.25		meas.				0.278	1.323	1.06	
	[(Pr.8, Nd.2)2 Fe14 B]																	
HZB CPMU15 under development for FEL	with GBD. VAC				2	15	130	2		2.14	design			in dev.	0.133	2.180	1.02	[49], [51]
HZB CPMU17 under development for BESSY	[(Pr.8, Nd.2)2 Fe14 B]	300 K	>1.38	>20.6	5.5	17	87.5	1.6			in dev.							[49], [52 - 53]
	with GBD. VAC	77 K	>1.62	>67.1						1.17	design			in dev.	0.324	1.133	0.97	
IHEP	PrFeB with GBD	<85 K	1.58	77.9	5	13.5	140	2	1		design	4.5 thick	2.25 thick	in dev.	0.370	0.968	0.97	[54 - 57]
NSLS short prototype	NMX 53CR (PrFeB)	77 K			4.85	14.5	8		0.9		meas.				0.334	1.092	1.21	[58]
	Neomax	300 K							0.75									
NSLS bakeable prototype	NMX-47CR (Pr ₂ Fe ₁₄ B	300 K	1.21	30	5	16.8	9.5		0.92		meas.	50X29X5.6	40X25.5X2.8		0.298			[59 - 60]
	Neomax	77K							1.049		meas.				0.298	1.237	1.18	
SOLEIL 4-period test. 2nd test.	NMX-53CR (Pr ₂ Fe ₁₄ B	293 K	1.35	16.5	10	18	4		0.367		meas.	50x30x6.5	33x22x2.5		0.556			[33 - 35]
	Neomax	77 K	1.57						0.435		meas.				0.556	0.528	1.21	
SOLEIL First full PrFeB/VP undulator	NMX-53CR (Pr ₂ Fe ₁₄ B	293 K	1.35	16.3	5.5	18	107		1.04		meas.	50x30x6.5	33x22x2.5	installed	0.306	1.204		[33, 34], [61 - 65]
for NANOSCOPIUM beamline	Neomax	77 K	1.57	76					1.152		meas.			Aug 2011	0.306	1.204	1.05	
SOLEIL U18n°2 cryo-ready und. for COXINEL																		
Installed; in use at room temp		293 K	1.317	24	5	18		2	1.156									[62, 63, 65, 66]
SOLEIL U18n°3 for ANATOMIX beamline						18		2			in dev.			end 2017				[65, 66]
SOLEIL U15 for PROXIMA II beamline, LUNEX5																		
collab. With MAX-LAB	NMX-53CR (Pr ₂ Fe ₁₄ B	77 K			3	15	200	3	1.67		design			in dev.	0.200	1.728	1.03	[62, 63, 65 - 67]
Taiwan Photon Source TPS	NMX-68CU (Pr ₂ Fe ₁₄ B	77 K	1.67	77.9	4	15	133	2	1.31	1.31	design	56x20x4.5	46x16x3	in dev.;	0.267	1.374	1.05	[3], [68 - 70]
		77 K			3					1.71	design			expected	0.200	1.728	1.01	
		293 K	1.4	21.1										June 2019				

Table 5. List of CPMUs based on magnets containing praseodymium (Pr). In the column labeled 'Ratio Calc/Meas', the measured value is used when available, otherwise the design value is used.

Table 6. List of NbTi-based SCUs at ANKA [17, 71 - 74] and APS [7, 8, 75 - 77]. All but the ANKA SCU20 coils and the LCLS R&D undulator have been operated with beam. The rightmost column gives the field strength calculated from Eq. 3, which uses the relevant magnetic gap and period and assumes operation at 80% of the critical current density.

NbTi SCU	Period (mm)	Gap (mm)	Magnetic Gap (mm)	B _{peak} (T)	B _{eff} (T)	Current (A)	% of I _c	Magnetic Length (m)	No. of Periods	Magnetic Gap/Period	Fit for NbTi SCU @ 80%
ANKA SCUDEMO	14	7	8	0.428		650			100	0.571	
ANKA SCU15	15	7	8	0.73		150	60		100.5	0.533	0.8687
ANKA SCU20 coils	20	7	8	1.187		395		1.5	75.5	0.400	1.5336
APS SCU0	16	7.2	9.5	0.7351	0.7321	600	72	0.33	21	0.594	0.7436
APS SCU1	18	7.2	9.5	0.9625	0.9611	450	78	1.08	60	0.528	0.9730
APS SCU2	18	7.2	9.5	0.9635	0.9624	450	78	1.08	60	0.528	0.9730
LCLS R&D undulator	21	5.7	8	1.67				1.5		0.381	1.6679

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